

INSTRUCTIONS

**TYPE TCF-10 POWER LINE CARRIER
FREQUENCY-SHIFT TRANSMITTER
10 WATT/10 WATT
FOR ALL RELAYING APPLICATIONS**

CAUTION: It is recommended that the user of this equipment become thoroughly familiar with the information in this instruction leaflet before energizing the carrier assembly. Failure to observe this precaution may result in damage to the equipment.

If the carrier set is mounted in a cabinet, it must be bolted down to the floor or otherwise secured before swinging out the equipment rack to prevent its tipping over.

APPLICATION

The type TCF-10 carrier transmitter equipment provides for the transmission of either of two closely controlled discrete frequencies, both within a narrow-band channel, over high-voltage transmission lines. The center frequency of the channel can vary from 30 to 300 KHz in 0.5 KHz steps. The two frequencies transmitted are separated by 200 Hz, one being at center frequency (fc) plus 100 Hz and the others at center frequency minus 100 Hz. The higher frequency, termed the Guard frequency, is transmitted continuously when conditions are normal. It indicates at the receiving end of the line that the channel is operative and it also serves to prevent false operation of the receiver by line noise. The lower frequency, termed the Trip frequency, is transmitted as a signal that an operation (such as tripping a circuit breaker) should be performed at the receiving end of the line.

When electro-mechanical relays are used for keying from guard to trip frequency, the contact

used is connected to the high voltage input of a buffering keying board. This board buffers the input so that random noise does not key the circuits. When solid state relays are used, the 20Vdc voltage used for keying is connected to the low voltage input of the buffering keying board.

CONSTRUCTION

The 10-watt/10-watt TCF-10 transmitter unit is mounted on a standard 19-inch wide chassis 5 $\frac{1}{4}$ inches (3 rack units) high with edge slots for mounting on a standard relay rack. Fuses, a pilot light, a power switch and a jack for metering the amplifier collector current are accessible from the front of the chassis when supplied. See Fig. 15. All of the circuitry that is suitable for printed circuit board mounting is on four such boards. The components mounted on each printed board or other sub-assembly are shown enclosed by dotted lines on the internal schematic, Fig. 1 or 2. The location of components on the four printed circuit boards are shown on separate illustrations, Fig. 3, 4, 5, 6 and 7.

External connections to the assembly are made through a 36-circuit receptacle, J3. The r.f. output connection to the assembly is made through a coaxial cable jack J2.

OPERATION

The transmitter is made up of four main stages and two filters. The stages include two crystal oscillators operating at frequencies that differ by the

All possible contingencies which may arise during installation, operation, or maintenance, and all details and variations of this equipment do not purport to be covered by these instructions. If further information is desired by purchaser regarding his particular installation, operation or maintenance of his equipment, the local Westinghouse Electric Corporation representative should be contacted.

desired channel frequency, a mixer and buffer amplifier, a driver stage and a power amplifier. One filter is located between the driver and the power amplifier and the filter removes harmonics that may be generated by distortion in the power amplifier.

A single crystal designed for oscillation in the 30 KHz to 300 KHz range cannot be forced to oscillate away from its natural frequency by as much as +100 Hz. In order to obtain this desired frequency shift, it is necessary to use crystals in the 2 MHz range. The crystals are Y1 and Y2 of Fig. 1. The frequency of Y2 is 2.00 MHz when operated with a specified amount of series capacity, and the frequency of Y1 is 2.00 MHz plus the channel frequency, or 2.03 MHz for a channel frequency of 30 KHz. Capacitor C55 and crystal Y2 in series are connected between the positive side of the supply voltage and the base of transistor Q51, which operates in the emitter follower mode. The emitter is coupled to the base through C57, and with Y2 removed the base of Q51 would be held at approximately the midpoint of the supply voltage by R51 and R52. The crystal serves as a series-resonant circuit with very high inductance and low capacitance. The circuit can be made to oscillate at other than the natural frequency of the crystal by varying the series capacitor, C55. Increasing C55 will lower the frequency of oscillations and reducing C55 will raise the frequency.

Crystal Y1 is connected in a circuit that is similar except for the addition of C53 and diodes D51 and D52. By adjustment of C52 this circuit is made to oscillate at 100 Hz above its marked frequency. Capacitor C53 is not effective until D51 is biased in the forward direction and becomes conductive. It is biased in the reverse direction until the relay control contact is closed, which places 45 Vdc at terminal 3 of the printed circuit board. With D51 conducting, C53 is effectively in parallel with C52, and adjustment of C53 will reduce the frequency by 200 Hz. The crystals taken individually have a greater variation of frequency with temperature than would be acceptable. However, by proper matching of the two crystals, the variation in their difference frequency can be kept within limits that permit holding the frequency stability of the overall transmitter to ± 10 Hz over a temperature range of -20 to +55°C.

The frequencies produced by the two oscillators are coupled to the base of mixer transistor Q53 through C62 and C63. The sum of the two frequencies is so high that a negligible amount appears on the secondary of transformer T51, but the difference frequency is accepted and amplified by Q53 and Q54.

When the relay control, or keying, contact is closed, it changes the frequency from Guard to Trip.

As is shown on the Internal Schematic, Fig. 1, the voltage for the keying circuit is obtained from the 45-volt regulated supply in the transmitter, and opening the single power switch de-energizes both the transmitter and the keying circuit.

The driver stage consists of transistors Q56 and Q57 connected in a conventional push-pull circuit with input supplied from the collector of Q54 through transformer T52.

The driver filter, FL101, consists of a series-resonant inductor and capacitor connected between the driver and power amplifier stages by appropriate transformers T1 and T2. This filter greatly improves the waveform of the signal applied to the power amplifier.

The power amplifier uses two series-connected power transistors, Q2 and Q4, operating as a class B push-pull amplifier with single-ended output. Diodes D2 and D4 provide protection for the base-emitter junctions of the power transistors. Zener diodes Z2 and Z4 protect the collector-emitter junctions from surges that might come in from the power line through the coaxial cable.

The output transformer T3 couples the power transistors to the output filter FL102. The output filter includes two trap circuits (L102, C1, C2 and L103, C3, C4) which are factory tuned to the second and third harmonics of the transmitter frequency. Capacitor C5, C6 approximately cancels the inductive reactance of the two trap circuits at the operating frequency. Protective gap G1 is a small lightning arrester to limit the magnitude of switching surges or other line disturbances reaching the carrier set through the line turner and coaxial cable. Auto-transformer T4 matches the

filter impedance to coaxial cables of 50, 60, or 70 ohms.

The series resonant circuit composed of L105 and C7 is tuned to the transmitter frequency, and aids in providing resistive termination for the output stage. Jack J102 is mounted on the front panel of FL102 and is used for measuring the r.f. output current of the transmitter into the coaxial cable. It should be noted that the filter contains no shunt reactive elements, thus providing a reverse impedance that is free of possible "across-the-line" resonances.

The power supply is a series-type transistorized dc voltage regulator which has a very low stand-by current drain when there is no output current demand.

The Zener diode Z1 holds a constant base-to-negative voltage on the series-connected power darlington transistor Q1. Depending on the load current, the dc voltage drop through transistor Q1 and resistor R1 and R2 varies to maintain a constant output voltage. The Zener diode Z2 when used serves to drop the 100v regulated supply to 45v for use with both the keying circuit and the external TCF voice adapter. It is placed in series so that it does not draw current unless called upon by the external voice adapter. Capacitor C3 provides a low carrier-frequency impedance across the dc output voltage. Capacitors C1 and C2 across the dc output voltage by pass r.f. or transient voltages to ground, thus preventing damage to the transistor circuit.

CHARACTERISTICS

Frequency Range	30-300 kHz
Output	10 watt guard - 10 watts trip - (into 50 to 70 ohm resistive load)
Frequency Stability	± 10 Hz from -20°C to +55°C.
Frequency Spacing	A. When used with narrow band receiver. 1. One-way channel, two or more signals-500 Hz min.

Harmonics	Down 55 db (min.) from output level.
Input Voltage	48 or 125 v.d.c.
Supply Voltage variation	42-56v. for nom. 48v. supply. 105-140v. for nom. 125v. supply.
Battery Drain	0.5 a guard } 1.15a. trip }
	48 v.d.c.
	0.2a. guard } 0.4a. trip }
	125 v.d.c.
Keying Circuit Current	4 ma.
Temperature Range	-20 to +55°C around chassis.
Dimensions	Panel height - 5 1/4" or 3 r.u. Panel width - 19"
Weight	12 lbs.

INSTALLATION

The TCF-10 transmitter is generally supplied in a cabinet or on a relay rack as part of a complete carrier assembly. The location must be free from dust, excessive humidity, vibration, corrosive fumes, or heat. The maximum ambient temperature around the chassis must not exceed 55°C.

ADJUSTMENTS

The TCF-10 10W/10W transmitter is shipped with the power output control R64 set for output

of 10 watts into a 60 ohm load. If it is desired to check the adjustments, or if repairs have made readjustment necessary, the coaxial cable should be disconnected from the assembly terminals and replaced with a 50 to 70 ohm non-inductive resistor of at least a 10 watt rating. Use the value of the expected input impedance of the coaxial cable and line tuner. If this is not known, assume 60 ohms. Connect the T4 output lead to the corresponding tap. Connect an ac vacuum tube voltmeter (VTVM) across the load resistor. Turn power output control R64 to minimum (full counter-clockwise). Turn on the power switch on the panel and note the power supply dc voltage. If this is in the correct range, rotate R64 clockwise to obtain 4 or 5 volts across the load resistor used. At this point check the adjustment of the series output tuning coil L105 by loosening the knurled shaft-locking nut and moving the adjustable core in and out a small amount from its initial position. Leave it at the point of maximum voltage across the load resistor used. Then rotate R64 farther clockwise to obtain the correct voltage for 10 watts in the load resistor, as shown in the following table.

Then change to Trip frequency by connecting together terminals 9 and 5 of J3 and connecting together terminals 4 and 12 of J3, and rotate R64 until the voltage across the load resistor is as shown in the following table for a 10 watt output. Recheck the adjustment of L105 for maximum output voltage and readjust R64 for a 10 watt output if necessary. Tighten the locking nut on L105. Open the power switch.

T106 Tap	Voltage for 10 Watts Output
50	22.4
60	24.5
70	26.5

Follow the procedure outlined in the line tuner instructions for its adjustment.

Normally the output filter (FL102) will require no readjustment except as noted above. It is factory tuned for maximum second and third harmonic rejection, and for series resonance (maximum output at the fundamental frequency) with a

60-ohm load. A small amount of reactance in the transmitter output load circuit may be tuned out by readjustment of the moveable core of L105. This may be necessary with some types of line coupling equipment. The adjustable cores of L102 and L103 have been set for maximum harmonic rejection and no change should be made in these settings unless suitable instruments are available for measuring the second and third harmonic present in the transmitter output.

The operating frequencies of crystals Y1 and Y2 have been carefully adjusted at the factory and good stability can be expected. If it is desired to check the frequencies of the individual crystals this can be done by turning the matched pair 180° and inserting a crystal in its proper socket with the other crystal unconnected. A sensitive frequency counter with a range of at least 2.3 MHz can be connected from TP51 to TP54. (Connection to TP54 rather than to TP53 provides a better signal to the counter and avoids some error from the effect of the counter input capacitance on the oscillator circuit.) While measurement of the oscillator crystals, individually is necessary for the initial adjustment of the oscillators, generally any subsequent checks may be made with a lower range counter connected at the transmitter output. If any minor adjustment of the Guard and Trip frequencies should be needed the Guard adjustment should be made with capacitor C52 and the Trip Adjustment with C53.

MAINTENANCE

Periodic checks of the transmitter Guard and Trip power outputs will detect impending failure so that the equipment can be taken out of service for correction. At regular maintenance intervals, any accumulated dust should be removed, particularly from the heat sinks. It is also desirable to check the transmitter power output at such times, making any necessary readjustments to return the equipment to its initial settings.

Voltage values should be recorded after adjustment in order to establish reference values which will be useful when checking the apparatus. The readings will remain fairly constant over an indefinite period unless a failure occurs. However, if transistors are changed, there may be considerable

difference in these readings without the overall performance being affected.

Typical voltage values are given in the following tables. Voltages should be measured with a VTVM. Readings may vary as much as $\pm 20\%$.

Note that values are given for 1 watt levels as well as 10 watt levels in case it is desired to operate the set at this reduced output level which in many applications may be preferable.

TABLE I TRANSMITTER DC MEASUREMENTS

Note: All voltages are positive with respect to Neg. dc (TP51). All voltages read with dc VTVM.

Test Point	Voltage at 1 Watt Output		Voltage at 10 Watts Output	
	48V units	125V units	48V units	125V units
TP52	20	20	20	20
TP53	5.4		5.4	
TP54	3.4		3.4	
TP55	21	20	18.5	18.5
TP56	21	20	18.5	18.5
TP57	<1.0		<1.0	
TP58	44.3	100	44.1	100
TP59	<1.0		<1.0	
TP101	0	0	0	0
TP103	21+2	50	21+2	50
TP105	44.3	100	44.0	100

TABLE II TRANSMITTER RF MEASUREMENTS

Note: Voltages taken with transmitter set of indicated output across 60 ohms. These voltages subject to variations depending upon frequency and transistor characteristics. T51-3 = Terminal 3 of transformer T51. Other transformer terminals identified similarly. All read with ac VTVM.

Test Point	Voltage at 1 watt Output	Voltage at 10 watts Output	48V	125V	48V
TP54 to TP51	0.015-0.03	0.015-0.03			
TP57 to TP51	0.05 -0.09	0.3 -1.2			
TP59 to TP51	0.05 -0.09	0.3 -1.2			
			48V	125V	48V
T1-1 to TP51		1.65			5.6
T1-3 to TP51		1.45			4.9
T1-4 to Gnd.		.6			2.0
T2-1 to Gnd.		.57			1.85
TP101-TP103		5.2			17.0
TP103 to TP105		5.2			17.0
T3-4 to Gnd.		35		35	112
T4-2 to Gnd.		31		31	110
TP109 to Gnd.		9.8		9.8	31
J102 to Gnd.		7.8		7.8	24.5

CONVERSION OF TRANSMITTER FOR CHANGED CHANNEL FREQUENCY

The parts required for converting a 10W/10W TCF transmitter for operation on a different channel frequency consist of a pair of matched crystals for the new channel frequency, new capacitors C103 and C104 on the power amplifier circuit board if the old and new frequencies are not in the same frequency group (see table on internal schematic drawing) and, in general, new or modified filters FL101 and FL102. Inductors L101, L102 and L103 in these filters are adjustable over a limited range, but forty-two combinations of capacitors and inductors are required to cover the frequency range of 30 to 300 kHz. The widths of the frequency groups vary from 1.5 kHz at the low end of the channel frequency range to 13 kHz at the upper end. A particular assembly can be adjusted over a somewhat wider range than the width of its assigned group since some overlap is necessary to allow for component tolerances. The nominal kHz adjustment ranges of the group are:

30.0-31.5	61.0- 64.0	113.0-119.5	207.1-214.0
32.0-33.5	64.5- 68.0	120.0-127.0	214.1-222.0
34.0-36.0	68.5- 72.0	127.5-135.0	222.1-230.0
36.5-38.5	72.5- 76.0	135.5-143.0	230.1-240.0
39.0-41.0	76.5- 80.0	143.5-151.0	240.1-250.0
41.5-44.0	80.5- 84.5	151.5-159.5	250.1-262.0
44.5-47.0	85.0- 89.0	160.0-169.5	262.1-274.0
47.5-50.0	89.5- 94.5	170.0-180.0	284.1-287.0
50.5-53.5	94.0-100.0	180.5-191.5	287.1-300.0
54.0-57.0	100.5-106.0	192.0-200.0	
57.5-60.5	106.5-112.5	200.1-207.0	

If the new frequency lies with the same frequency group as the original frequency, the filters can be readjusted. If the frequencies are in different groups, it is possible that changes only in the fixed capacitors may be required. In general, however, it is desirable to order complete filter assemblies adjusted at the factory for the specified frequency.

A signal generator, a frequency counter and a vacuum tube voltmeter are required for readjustment of FL101. The signal generator and the counter should be connected across terminal 4 and 5 of transformer T1 and the voltmeter across terminals 1 and 2 of transformer T2. The signal generator should be set at the channel center frequency and at 2 to 3 volts output. The core screw of the small inductor should be turned to the position that gives a true **maximum** reading on the VTVM. Turning the screw to either side of this position should definitely reduce the reading. The change in inductance with core position is less at either end of the travel than when near the center and consequently the effect of core screw rotation on the VTVM reading will be less when the resonant inductance occurs near the end of core travel.

The procedure for readjustment of the 2nd and 3rd harmonic traps of filter FL102 is somewhat similar. A signal generator and a counter should be connected to terminals 3 and 4 of transformer T3, and a 500 ohm resistor and a VTVM to the terminals of protective gap G1. The ground or shield lead of all instruments should be connected to the ground terminal of the transformer. Set the signal generator at exactly twice the channel center frequency and at 5 to 10 volts output. Turn the core screw of the large inductor L102, to the position that gives a definite **minimum** reading on the VTVM. Similarly, with the signal generator set at

exactly three times the channel center frequency and 5 to 10 volts output, set the core screw of the small inductor, L103, to the position that gives a definite **minimum** reading on the VTVM. Then remove the instruments and the 500 ohm resistor.

After the new pair of matched crystals have been adjusted, as described under "ADJUSTMENTS", the transmitter can be operated with a 50 to 70 ohm load (depending on which tap of T4 is used) connected to its output, and inductor L105 can be readjusted for maximum output at the changed channel frequency by the procedure described in the same section.

If a frequency-sensitive voltmeter is available, the 2nd and 3rd harmonic traps may be adjusted without using an oscillator as a source of double and triple the channel frequency. Connect the frequency-sensitive voltmeter from TP109 to ground and adjust the transmitter for rated output into the selected load resistor. Set the voltmeter at twice the channel frequency and, using the tuning dial and db range switch, obtain a maximum on-scale reading of the 2nd harmonic. Then vary the core position of L102 until a minimum voltmeter reading is obtained. Similarly, tune the voltmeter to the third harmonic and adjust L103 for minimum voltmeter reading. Although the transmitter frequency will differ from the channel center frequency by 100 Hz, the effect of this difference on the adjustment of the harmonic traps will be negligible. It should be noted that the true magnitude of the harmonics cannot be measured in this manner because of the preponderance of the fundamental frequency at the voltmeter terminals. Accurate measurement of the harmonics requires use of a filter between TP109 and the voltmeter that provides high rejection of the fundamental. The insertion losses of this filter for the 2nd and 3rd harmonics must be measured and taken into account.

RECOMMENDED TEST EQUIPMENT

- I. Minimum Test Equipment for Installation.
 - a. 60-ohm 10-watt non-inductive resistor.
 - b. A-C vacuum Tube Voltmeter (VTVM). Voltage range 0.003 to 30 volts, frequency range 60 hz to 330 kHz; impedance 7.5 megohms.

c. D-C vacuum Tube Voltmeter (VTVM).

Voltage Range: 1.5 to 300 volts.
Input Impedance 7.5 megohms.

II. Desirable Test Equipment for Apparatus Maintenance.

a. All items listed in I.

b. Signal Generator

Output Voltage: up to 8 volts.
Frequency Range: 20-kHz to 900 kHz

c. Oscilloscope

d. Frequency counter

e. Ohmmeter

f. Capacitor checker.

Some of the functions of the recommended test equipment are combined in the type TCT carrier test meter unit, which is designed to mount on a standard 19" rack but also can be removed and used as a portable unit.

RENEWAL PARTS

Repair work can be done satisfactorily at the factory. However, replacement parts can be furnished, in most cases, to customers who are equipped for doing repair work. When ordering parts, always give complete nameplate data and identify the part by its designation on the Internal Schematic drawing.

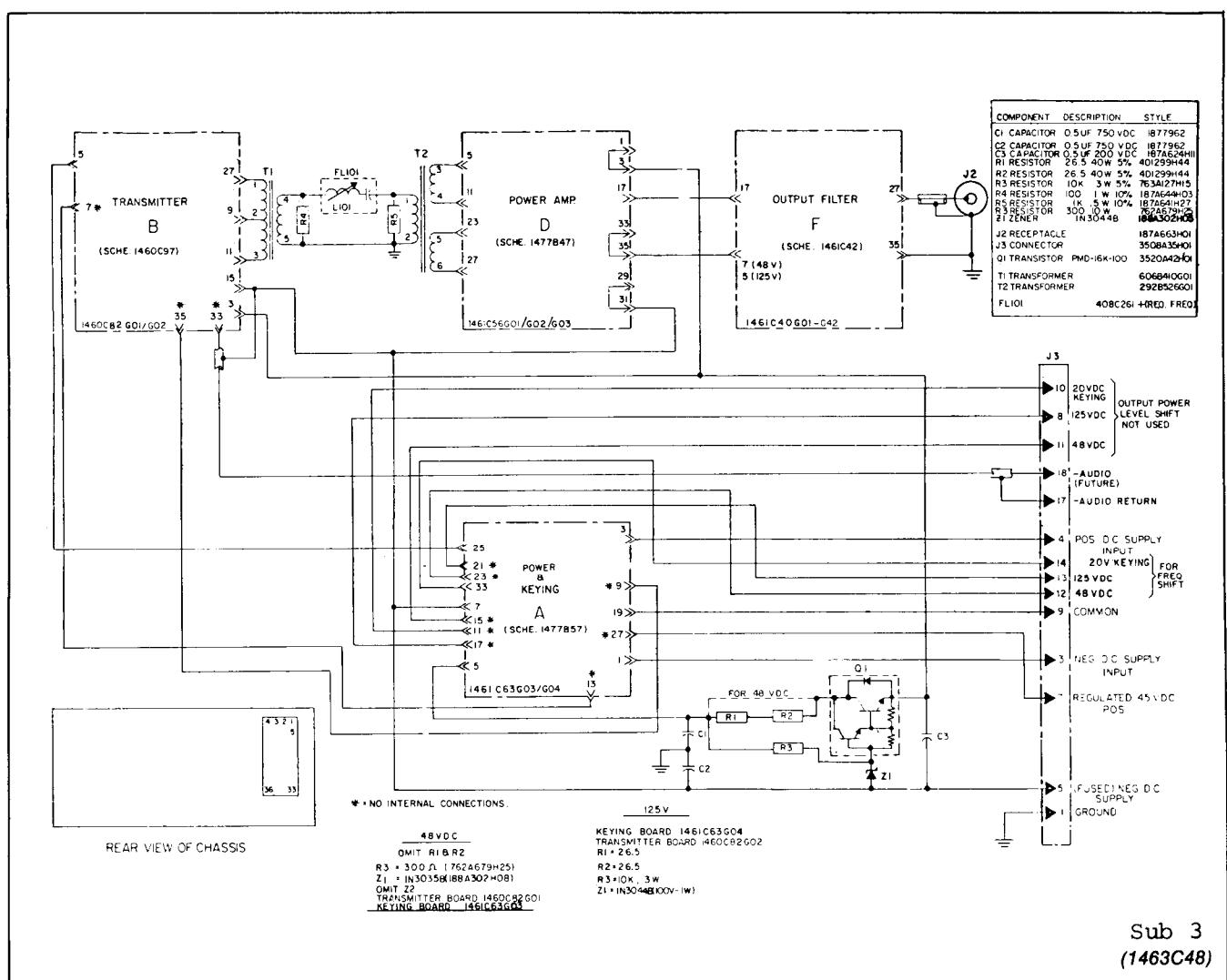
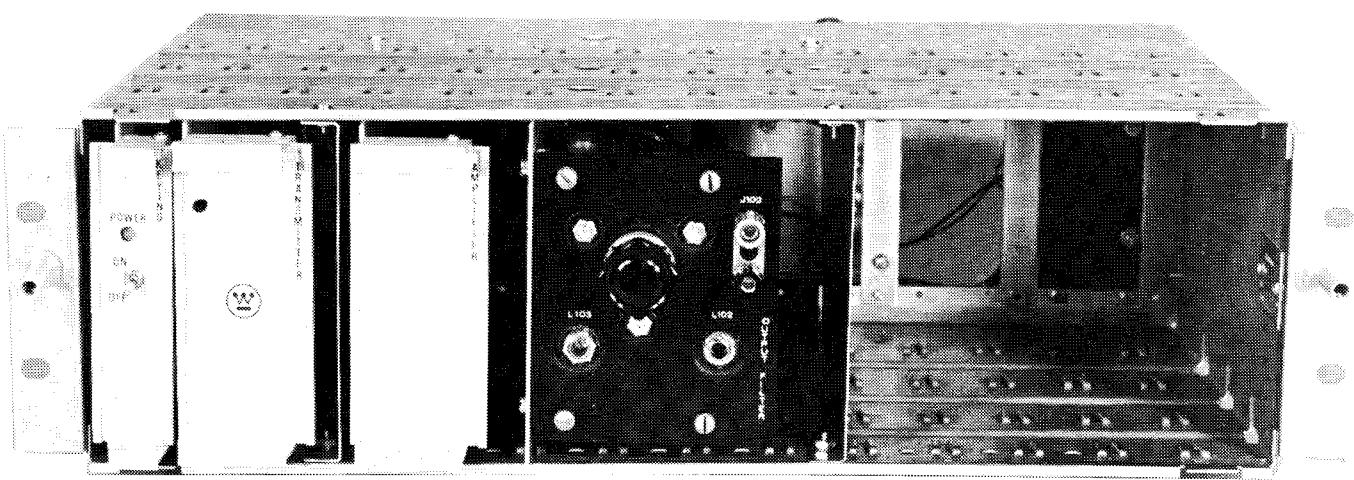
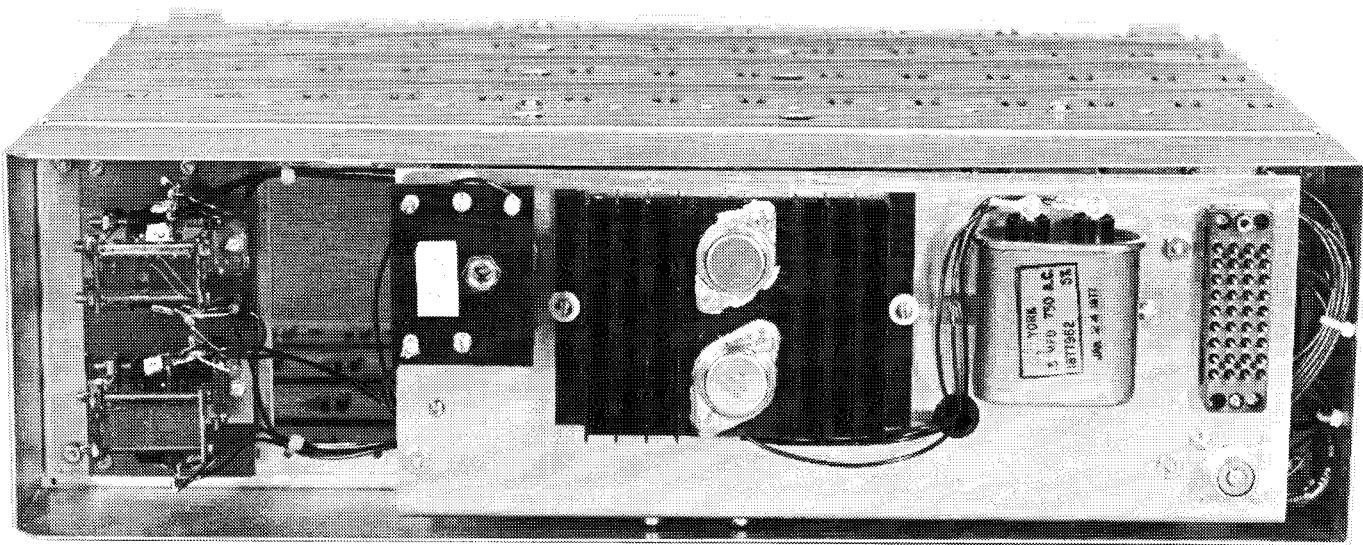


Fig. 1. Internal Schematic of Type TCF-10 Transmitter - With Switch, Pilot Light, and Fuses.



TCF-10 TRANSMITTER (Front View)



TCF-10 TRANSMITTER (Rear View)

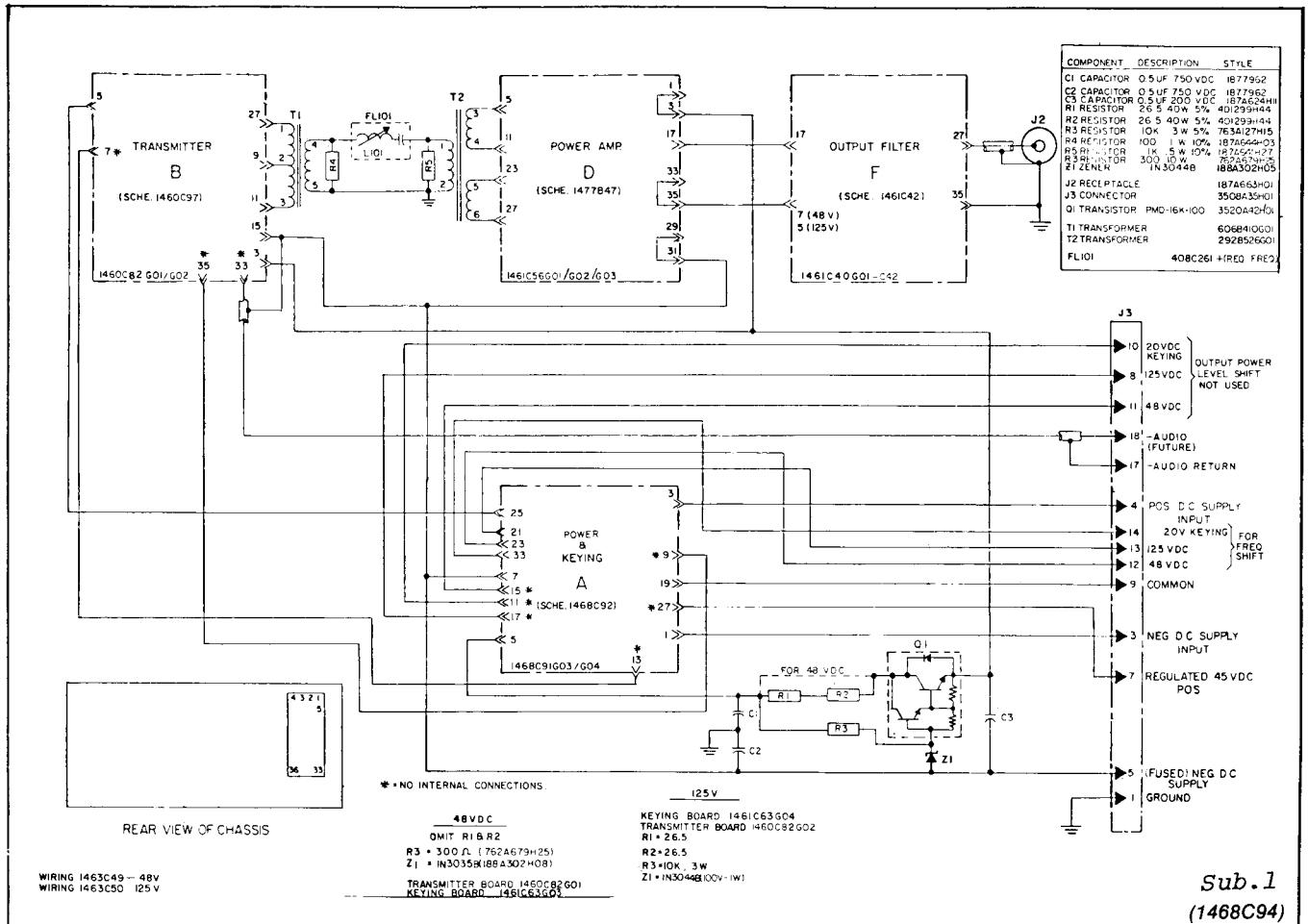


Fig. 2. Internal Schematic of Type TCF-10 Transmitter - Without Switch, Pilot Light and Fuses but with Mark & Space Pushbuttons.

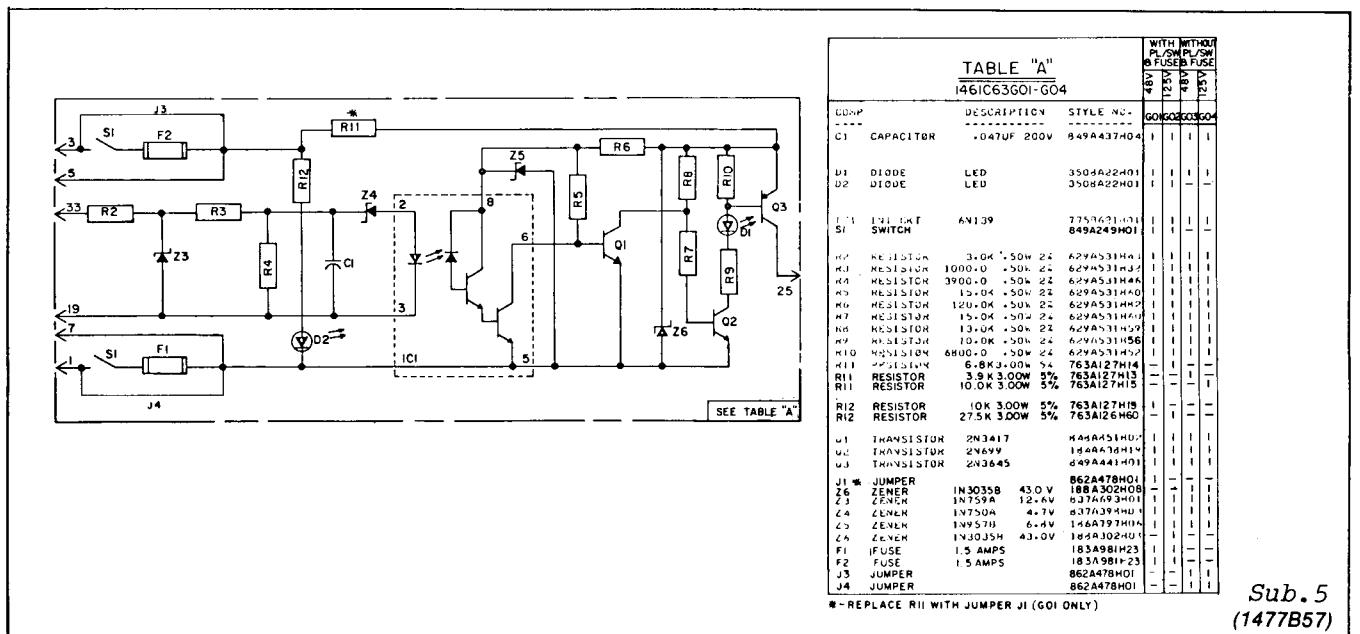


Fig. 3. Internal Schematic Keying Board.

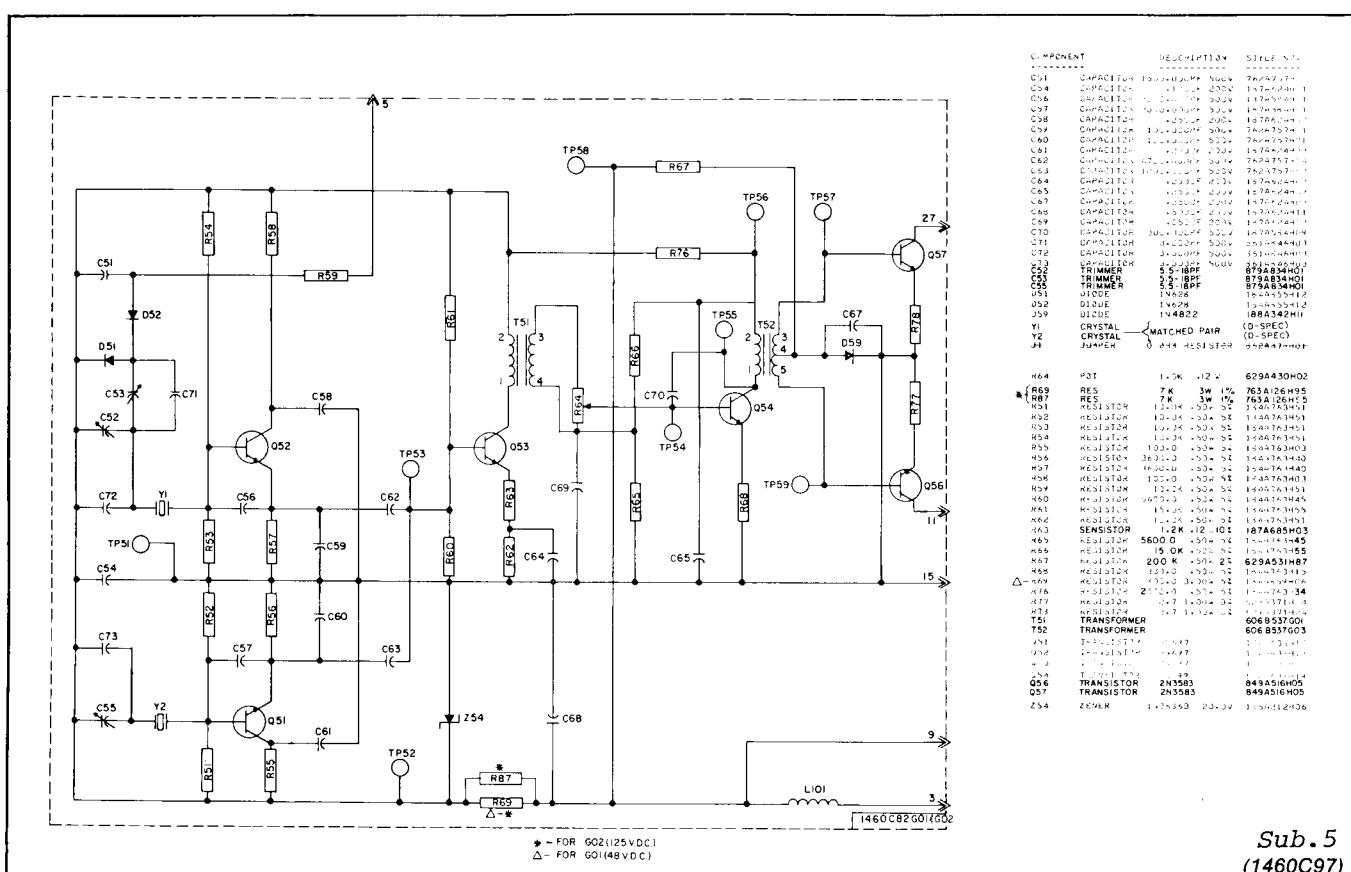


Fig. 4. Internal Schematic Transmitter Board.

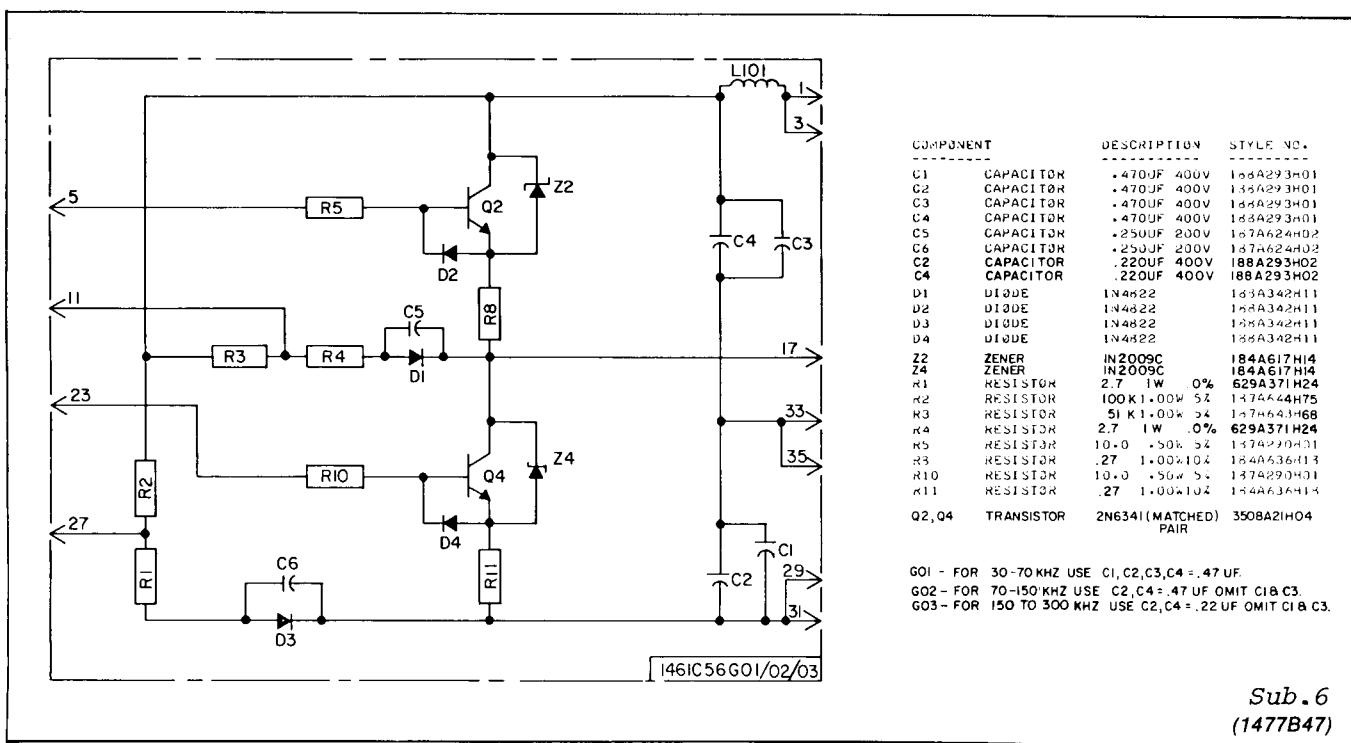


Fig. 5. Power Amplifier Board.

COMPONENT	DESCRIPTION	STYLE
C1 CAPACITOR	250PF MMF .500V	86-084644000
C2 CAPACITOR	100PF MMF .500V	86-084645000
C3 CAPACITOR	150PF MMF .500V	76Z-AT57H000
C4 CAPACITOR	3300 PF MMF .500V	17Z-AT58H026
C5 CAPACITOR	4000 PF MMF .500V	18T-AT70S15
C6 CAPACITOR	4000 MMF 120V C	18T-AT70S15
C7 CAPACITOR	7000 PF 3000V	20Z-ATC2H24
LI02 POT CORE		670B131000
LI03 POT CORE		670B131000
LI05 COIL		29ZB08EG00
T3 TRANSFORMER		29ZB525Q00
T4 TRANSFORMER		29ZB525Q00
R6 RESISTOR	3K * 5% BW12 REQ	180A3J7H01
R7 RESISTOR	15K 10% 2W	17D4624H5
GI LIGHTNING ARRESTER		87TA1000

COMPONENT	DESCRIPTION	STYLE
C1 CAPACITOR	2500 MMF 500V	86A46H20
C2 CAPACITOR	2000 MMF 500V	187A58H1
C3 CAPACITOR	1000 MMF 500V	767A75H20
C4 CAPACITOR	3300 MMF 500V	187A58H2
C5 CAPACITOR	2500 MMF 1200V	187A75H13
C6 CAPACITOR	5000 MMF 1200V	187A75H25
C7 CAPACITOR	6000 PPF 3000V	201C87Z28
L02 POT CORE		670B13504
L03 POT CORE		670B13506
L05 COIL		292B0E06
T3 TRANSFORMER		292B52504
T4 TRANSFORMER		292B52603
R6 RESISTOR	3K ± 5% .8W (2 REQ)	188A317H01
R7 RESISTOR	15K 10% 2W	187N164G
G1 LIGHTNING ARRESTER		877A18H01

COMPONENT	DESCRIPTION	STYLE
C1	CAPACITOR 2000 MMF 500 V	18T524H01
C2	CAPACITOR 2000 MMF 500 V	18T524H01
C3	CAPACITOR 390 MMF 500 V	76.2A745H01
C4	CAPACITOR 3300 MMF 500 V	18T524H01
C5	CAPACITOR 2500 MMF 1200 V	87A705H03
C6	CAPACITOR 4000 MMF 1200 V	18T4705H03
C7	CAPACITOR 5500 PF 300V	20C1872H2Z
L02	POT CORE	67B131C04
L03	POT CORE	67B131C06
L05	COIL	29B208E-01
T3	TRANSFORMER	29ZB202-04
T4	TRANSFORMER	29ZB2526G01
R6	RESISTOR 3K-.5% BW (2 REQ)	18GA317H01
R7	RESISTOR 15K 10% 2W	18T642H55
G1	LIGHTNING ARRESTER	87TA16H01

COMPONENT	DESCRIPTION	STYLE
C1 CAPACITOR	.1500 MFD 500V	762757H03
C2 CAPACITOR	.2000 MFD 500V	187548AHO1
C4 CAPACITOR	.3500 MFD 500V	187454H04
C5 CAPACITOR	.3000 MFD 250V	187457H03
C6 CAPACITOR	.2500 MFD 250V	187455H13
C7 CAPACITOR	.5000 PF 3000V	202C872H26
L02 POT CORE		670B13104
L03 POT CORE		673B13506
L05 COIL		292B06600
T3 TRANSFORMER		292B52604
T4 TRANSFORMER		292B52603
R6 RESISTOR	3K 1% HW (2 REQ)	186A317H01
R7 RESISTOR	15K 10% 2W	187464H55
GI LIGHTNING ARRESTER		877A1H01

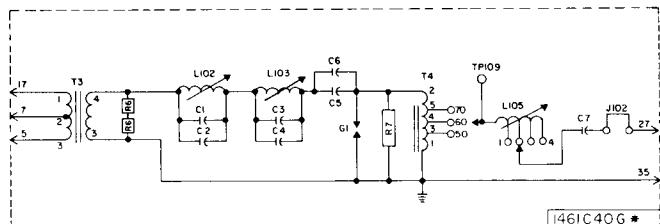


FIG. I
30 TO 200 KC

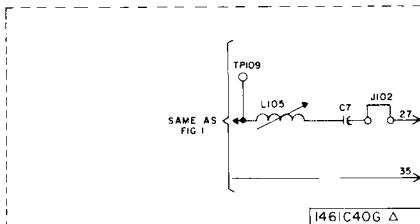


FIG.2 (OTHERWISE SAME AS FIG.1)
TO 300 KC ASSEMBLY: 14G1CH

* - GOI THRU G32
G43 THRU G74

△- G33 THRU G42
G75 THRU G84

C ASSEMBLY - 1461C4
COMP LOC - 1477B20
PC B - 1461C4

Sub 5
(1461C42)

Fig. 6. Internal Schematic Output Filter.

COMPONENT	DESCRIPTION	STYLE
C1 CAPACITOR	3000 MMF 500V	1874584H06
C3 CAPACITOR	B20 MMF 500V	762A757H22
C4 CAPACITOR	2000 MMF 500V	1874584H01
C5 CAPACITOR	2500 MMF 1200V	18747C5K13
C6 CAPACITOR	2500 MMF 1200V	18747D103H3
C7 CAPACITOR	4200 PF 3000V	1874C872V25
LIQ2 POT CORE		670B13C304
LIQ3 POT CORE		670B13C306
LIQ5 COIL		292B066001
T3 TRANSFORMER		292B525C4
T4 TRANSFORMER		292B526C03
R6 RESISTOR	3K ± 5% .8W (2 REQ)	198A317HO1
R7 RESISTOR	15K 10% 2W	187A642V155
GI LIGHTNING	ARRESTER	877A111C01

COMPONENT	DESCRIPTION	STYLE
C1	CAPACITOR 2500 MMF 500V	661A4B6H20
C2	CAPACITOR 150 MMF 500V	661A4B6H25
C3	CAPACITOR 150 MMF 500V	661A4B6H25
C5	CAPACITOR 200 MMF 1200V	137A705H04
C6	CAPACITOR 4000 MMF 1200V	137A705H15
C7	CAPACITOR 3500 PF 5000V	201C872423
L102	POT CORE	673B13C04
L103	POT CORE	673B13C06
L105	COIL	292B06001
T3	TRANSFORMER	292B526C4
T4	TRANSFORMER	292B525G03
R6	RESISTOR 34.2% 5W .8W (2 REQ)	(86A317H01)
R7	RESISTOR 15K 10% 2W	1781642A155
GI	LIGHTNING ARRESTER	877A16H01

COMPONENT	DESCRIPTION	STYLE
C1 CAPACITOR	3000 MMF 500V	187A584H09
C2 CAPACITOR	2000 MMF 500V	187A584H09
C3 CAPACITOR	1000 MMF 500V	762J584H09
C4 CAPACITOR	2000 MMF 500V	5040H041
C5 CAPACITOR	1500 MMF 1200V	187J73C911
C6 CAPACITOR	2000 MMF 1200V	187A705H12
C7 CAPACITOR	3200 PF 300CV	2018C721422
L102 POT CORE		679B13J004
L103 POT CORE		670B13J006
L105 COIL		292E06H01
T3 TRANSFORMER		292B526-C4
T4 TRANSFORMER		292B526G03
R6 RESISTOR	3K ± 5% BW (2 REQ)	188A317H01
R7 RESISTOR	1K5 10% 2W	187H64J155
G1 LIGHTNING ARRESTER		877A16H01

COMPONENT	DESCRIPTION	STYLE
C1 CAPACITOR	30 MMF 500V	763A2209H2
C2 CAPACITOR	2000 MMF 500V	187A584H01
C3 CAPACITOR	390 MMF 500 V	762A757H15
C4 CAPACITOR	1500 MMF 500 V	762A757H03
C5 CAPACITOR	3000 MMF 200 V	187A470H54
C6 CAPACITOR	200 MMF 200 V	187A470H54
C7 CAPACITOR	2800 PF 300V	202C672H40
L02 POT CORE		670B133G04
L03 POT CORE		670B133G05
L05 COIL		292B016G01
T3 TRANSFORMER		292B526G04
T4 TRANSFORMER		292B526G03
R6 RESISTOR	3K ± 5% 8W (2 REQ)	188A317H01
R7 RESISTOR	15K 10% 2W	187A64425K05
GI LIGHTNING ARRESTER		877AII6H01

1416140 G09 G51			
COMPONENT	DESCRIPTION	ST'LE	QTY
C1 CAPACITOR	300M MMF 500V	187A58H49	0.9
C2 CAPACITOR	150M MMF 500V	762A757H03	0.9
C3 CAPACITOR	180M MMF 500V	187A757H10	0.9
C4 CAPACITOR	150M MMF 500V	762A757H03	0.9
C5 CAPACITOR	200M MMF 1200V	187A7C5H15	0.9
C7 CAPACITOR	2200 PF 3000V	203C872H17	0.9
L102 POT CORE		670B13X204	0.9
L103 POT CORE		670B13X506	0.9
L105 COIL		292B086G01	0.9
T3 TRANSFORMER		292B856X04	0.9
T4 TRANSFORMER		292B856Z03	0.9
R6 RESISTOR	3K ± 5% 8W 12 REQ	188A31TH01	0.9
R7 RESISTOR	15K 10% 2W	187A642H55	0.9
G1 LIGHTNING ARRESTER		877A10E01	0.9

COMPONENT	DESCRIPTION	STYLE
C1 CAPACITOR	82 MF MF 500V	763A209H23
C2 CAPACITOR	1500 MFM 500V	762A757H03
C4 CAPACITOR	1500 MFM 500V	762A757H03
C5 CAPACITOR	3000 MFM 1200V	187A705H04
C6 CAPACITOR	500 MFM 1200V	187A705H04
C7 CAPACITOR	3500 PF 3000V	203C8172/23
L102 POT CORE		670B133C04
L103 POT CORE		670B133C06
L105 COIL		292B601G01
T3 TRANSFORMER		292B562G04
T4 TRANSFORMER		292B563G03
R6 RESISTOR	3K ± 5% 8W (2 REQ)	[393A17H03]
R7 RESISTOR	10K 10% 2W	187A642H155
G1 LIGHTNING ARRESTER		877A16H00

COMPONENT	DESCRIPTION	STYLE
C1 CAPACITOR	1000 MMF 500 V	762A757HQ2
C2 CAPACITOR	350 MMF 500 V	762A757H15
C3 CAPACITOR	1000 MMF 500 V	762A757H05
C4 CAPACITOR	300 MMF 500 V	187A584M09
C5 CAPACITOR	3000 MMF 1200V	187A7C5114
C7 CAPACITOR	300 PF 3000V	203CB72H21
L102 POT CORE		670B133E04
L103 POT CORE		673B133J06
L105 COIL		292B086G00
T3 TRANSFORMER		292B525G04
T4 TRANSFORMER		292B525J03
R6 RESISTOR	3K ±5% BW (2 REQ)	183A171H01
R7 RESISTOR	1K5 10% 2W	187A642H55
GI LIGHTNING ARRESTER		877A16H01

COMPONENT	DESCRIPTION	STYLE
C1 CAPACITOR	1000 MMF 500V	762A75TH02
C2 CAPACITOR	250 MMF 500V	866A846HII
C3 CAPACITOR	1000 MMF 500V	762A75TH02
C4 CAPACITOR	1000 MMF 500V	762A75TH02
C5 CAPACITOR	300 MMF 600V	873A75H03
C6 CAPACITOR	2500 MMF 1200V	1873A705M13
C7 CAPACITOR	2800 PF 3000V	201C872H20
L102 POT CORE		670B33G04
L103 POT CORE		670E133G04
L105 COIL		292B8R6G0
T3 TRANSFORMER		292B526G04
T4 TRANSFORMER		292B526G03
R6 RESISTOR	3K ± 5% BW (2 REO)	188A317H01
R7 RESISTOR	15K 10% 2W	187A542K56
GI LIGHTNING ARRESTER		B77A116H01

<u>COMPONENT</u>	<u>DESCRIPTION</u>	<u>STYLE</u>
C1 CAPACITOR	1000 MFD .005 V	762A75TH02
C2 CAPACITOR	1000 MFD .005 V	762A75TH01
C3 CAPACITOR	1000 MFD .005 V	762A75TH01
C4 CAPACITOR	36 MFD .005 V	763A209H4
C5 CAPACITOR	2500 MFD 1200V	IR7A705H1
C7 CAPACITOR	2500 PF 3000V	2C3C872H19
LI02 POT CORE		670B133G04
LI03 POT CORE		670B133G06
LI05 COIL		292B086G01
T3 "TRANSFORMER		292B526G04
T4 "TRANSFORMER		292B526G02
R6 RESISTOR	3K ± 5% RW (2 REQ)	I8EA317H01
R7 RESISTOR	15Ω 10% 2W	1B76424H25

COMPONENT	DESCRPTION	STYLE
C1 CAPACITOR	360 MF 500V	7624757H14
C2 CAPACITOR	620 MF 500V	1874A506
C3 CAPACITOR	820 MF 500V	7624757H22
C4 CAPACITOR	100 MF 500V	7624757H01
C5 CAPACITOR	200 MF 1200V	187A7C57-104
C6 CAPACITOR	2000 MMF 200V	187A0701H2
C7 CAPACITOR	2200 PF 300CV	203CB72P-001
L02 POT CORE		670B13J3C04
L13S POT CORE		670B13J3G06
L105 COIL		292B08E6.001
T3 TRANSFORMER		292B5625C04
T4 TRANSFORMER		292B5625C03
R6 RESISTOR	3K ± 5% 8W (2 REQ)	186A317H01
R7 RESISTOR	15K 10% 2W	137A644L55
C8 LIGHTNING ARRESTER		872A1KU01

COMPONENT	DESCRIPTION	STYLE
C1 CAPACITOR	250 MMF 500V	861A846HII
C2 CAPACITOR	620 MMF 500V	187A564HII
C3 CAPACITOR	820 MMF 500V	187A575H2
C5 CAPACITOR	1500 MMF 1200V	187A375HII
C7 CAPACITOR	2000 PF 300CV	203C872HII
L1#2 POT CORE		670B133C04
L1#3 POT CORE		670B131706
L1#5 COIL		292B060G01
T3 TRANSFORMER		292B523C04
T4 TRANSFORMER		292B525C04
R6 RESISTOR	3K ± 5% BW (2 REQ)	188A317H01
R7 RESISTOR	15K ± 10% BW	187A164Z455
SL LIGHTNING ARRESTER		877A16H01

COMPONENT	DESCRIPTION	LINE
C1 CAPACITOR	180 MMF 500V	762A75TH0
C2 CAPACITOR	620 MMF 500V	187A584HH
C3 CAPACITOR	130 MMF 500V	762A75TH07
C4 CAPACITOR	620 MMF 500V	187A584HH
C5 CAPACITOR	300 MMF 1200V	187A745H0G
C6 CAPACITOR	1500 MMF 1200V	187A745TH11
C7 CAPACITOR	1800 PF 300GV	203C82B7D
L03 POT CORE		67C133G04
L13 POT CORE		67C133G06
L03S COIL		292B086GG1
T3 TRANSFORMER		292B526G04
T4 TRANSFORMER		292B526G05
R6 RESISTOR	3K ± 5% 8W (2 REQ)	188A317H01
R7 RESISTOR	15K 10% 2W	197A642G55
GI LIGHTNING ARRESTER		877A16H01

1461C40G41,6B3			1461C40G42,6B4		
COMPONENT	DESCRIPTION	STYLE	COMPONENT	DESCRIPTION	STYLE
C1 CAPACITOR	MMF 500V	763A209H07	C2 CAPACITOR	MMF 500V	861A846H25
C2 CAPACITOR	MMF 500V	861A846H25	C3 CAPACITOR	MMF 500V	763A209H23
C3 CAPACITOR	MMF 500V	762A757H01	C4 CAPACITOR	MMF 500V	763A209H07
C4 CAPACITOR	MMF 500V	763A209H07	C5 CAPACITOR	MMF 1200V	187A705H08
C5 CAPACITOR	MMF 1200V	187A705H08	C7 CAPACITOR	PF 3000V	203C872H02
C7 CAPACITOR	PF 3000V	203C872H02	L102 POT CORE	670B133G09	670B133G09
L102 POT CORE	670B133G08	670B133G08	L103 POT CORE	670B133G09	670B133G09
L103 POT CORE	670B133G09	670B133G09	T3 TRANSFORMER	292B526G04	292B526G04
T3 TRANSFORMER	292B526G04	292B526G03	T4 TRANSFORMER	292B526G04	292B526G03
R6 RESISTOR	3K ± 5% BW (2 REQ)	188A317H01	R6 RESISTOR	3K ± 5% BW (2 REQ)	188A317H01
R7 RESISTOR	15K 10% 2W	187A642H55	R7 RESISTOR	15K 10% 2W	187A642H55
G1 LIGHTNING ARRESTER		877AI16HO1	G1 LIGHTNING ARRESTER		877AI16HO1

PARTS LIST & SCHEMATIC - SHEETS 1 THRU 5 - DRAWING 1461C42

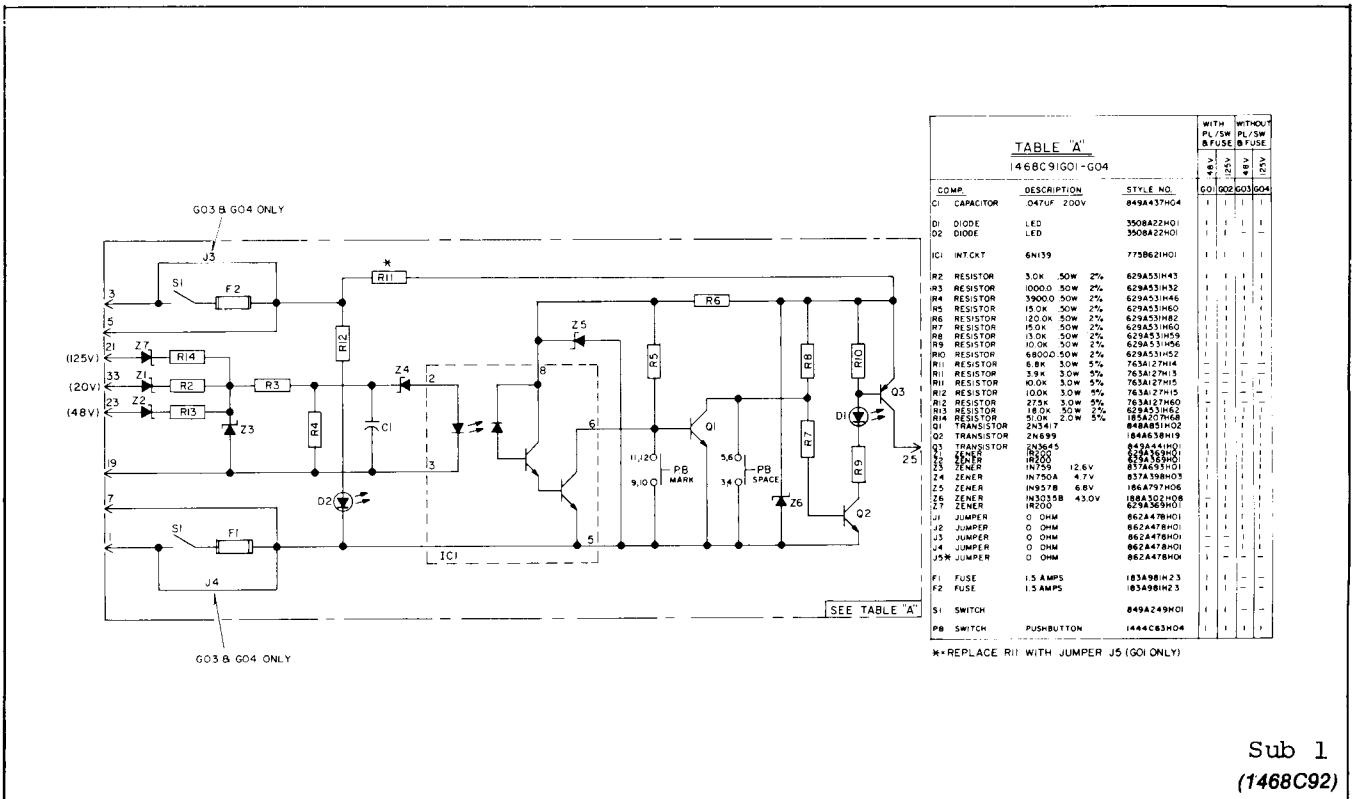


Fig. 7. Internal Schematic Keying Board with Pushbutton.

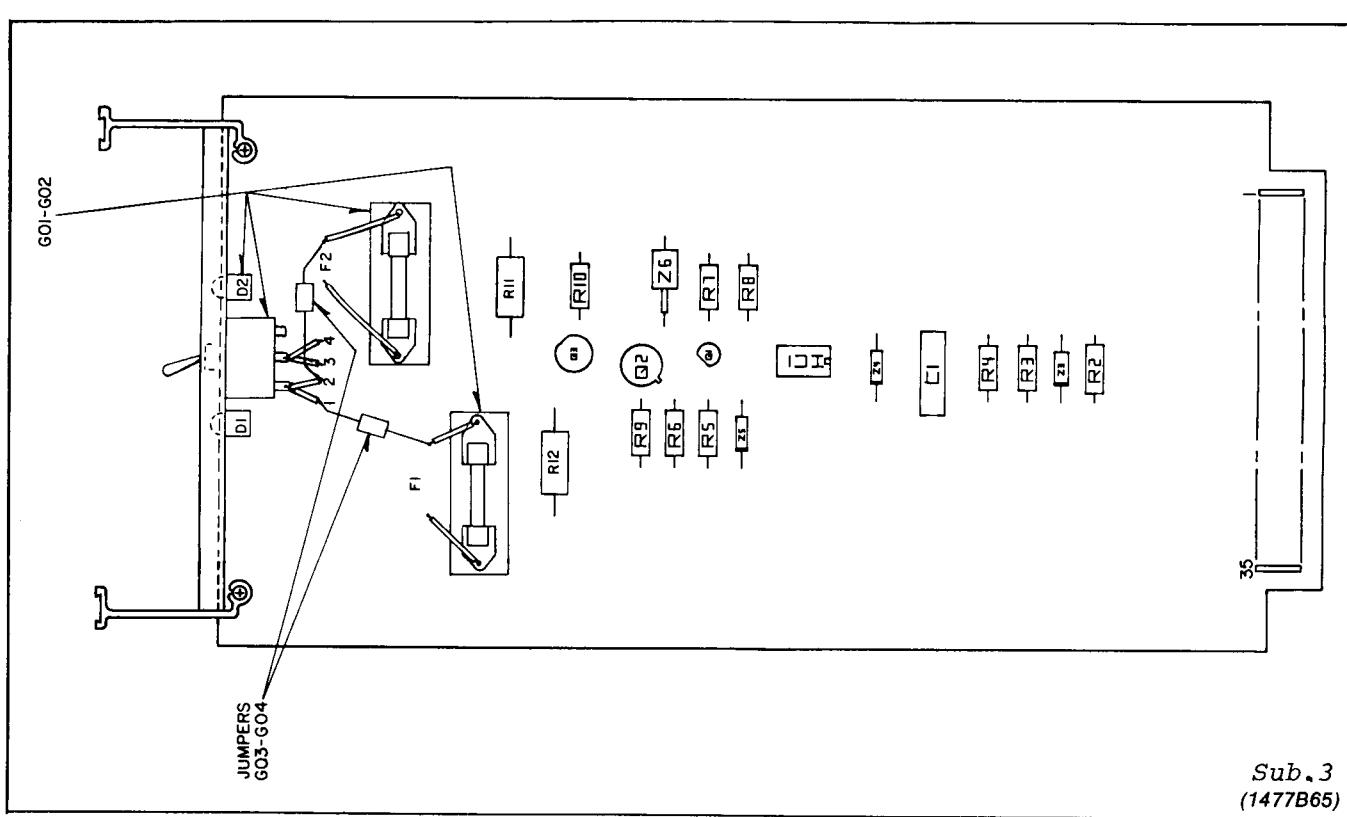


Fig. 8. Component Location Keying Board.

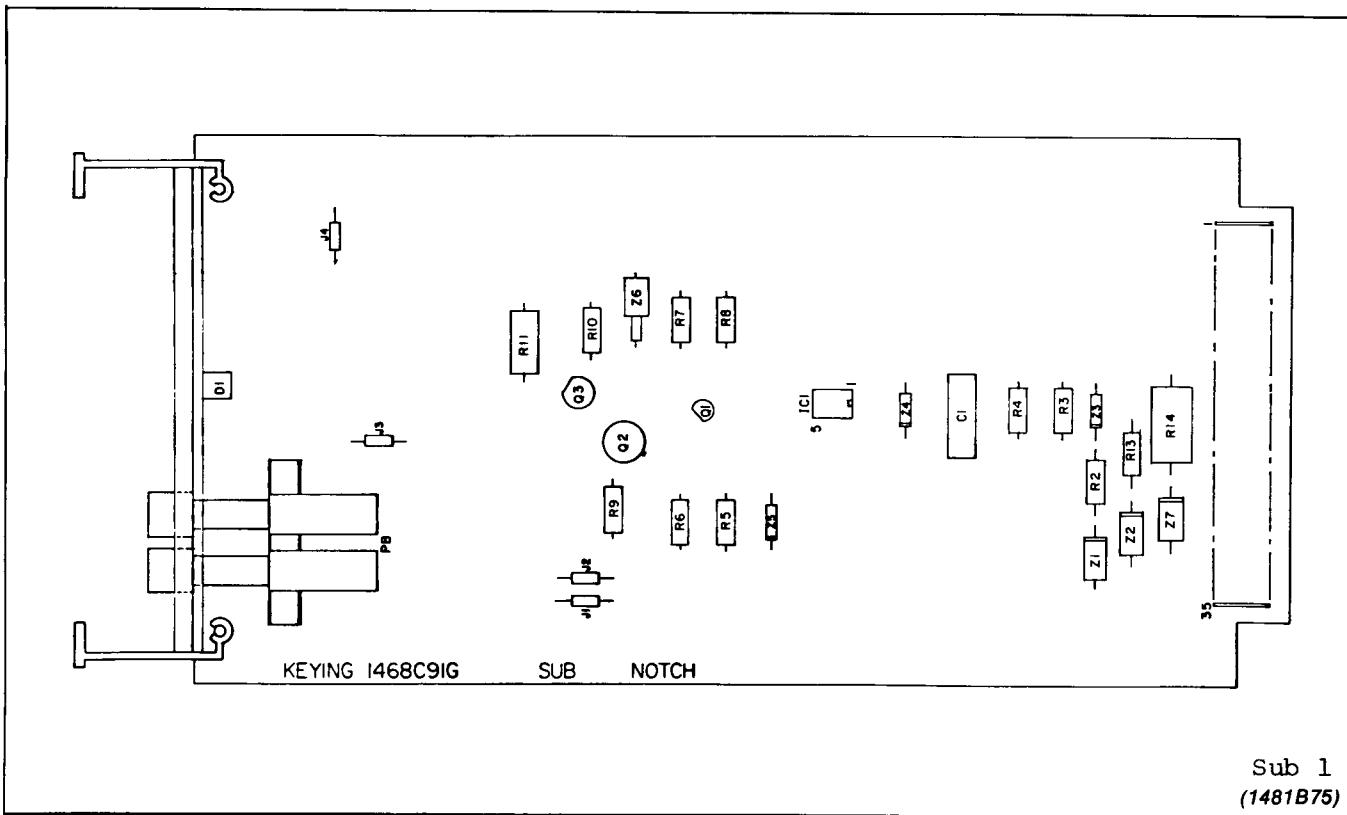


Fig. 9. Component Location Keying Board with Pushbuttons.

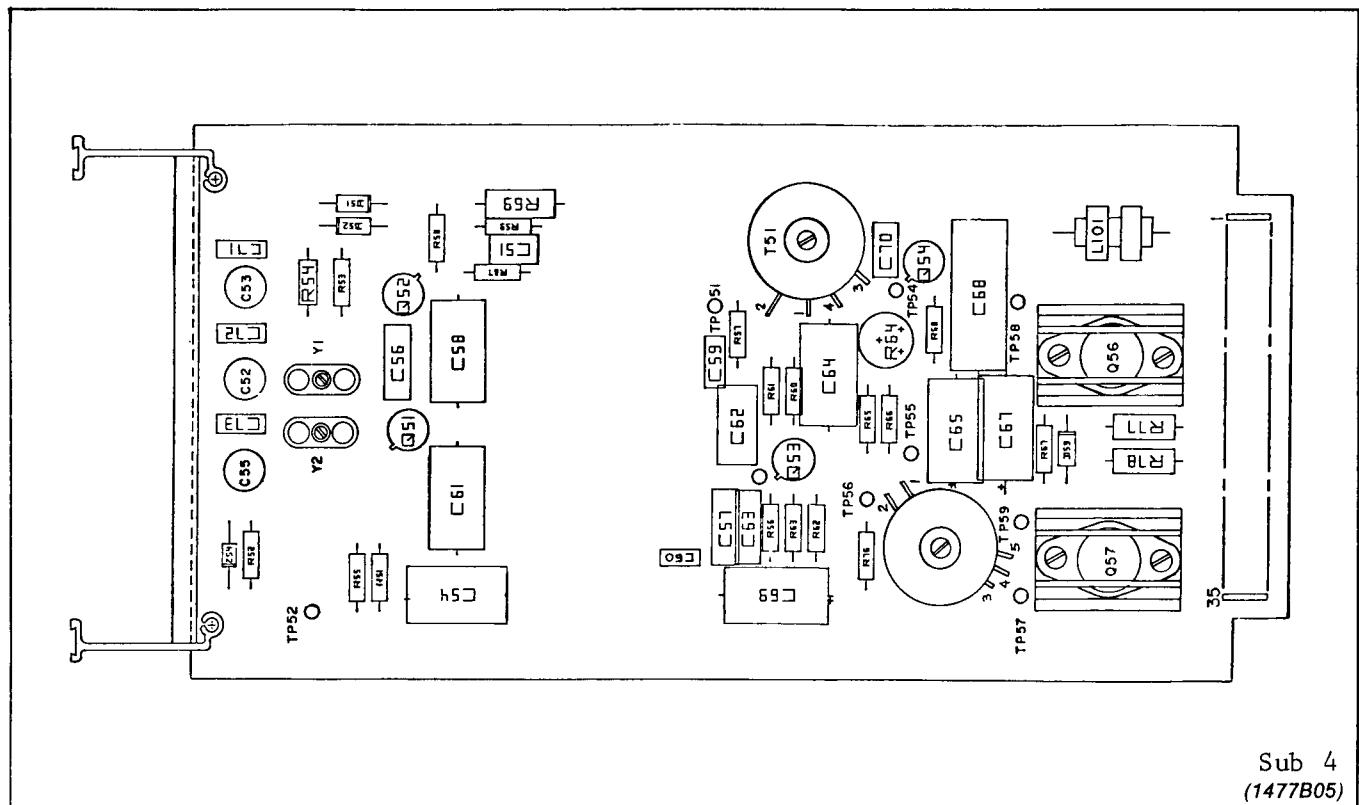


Fig. 10. Component Location Transmitter Board.

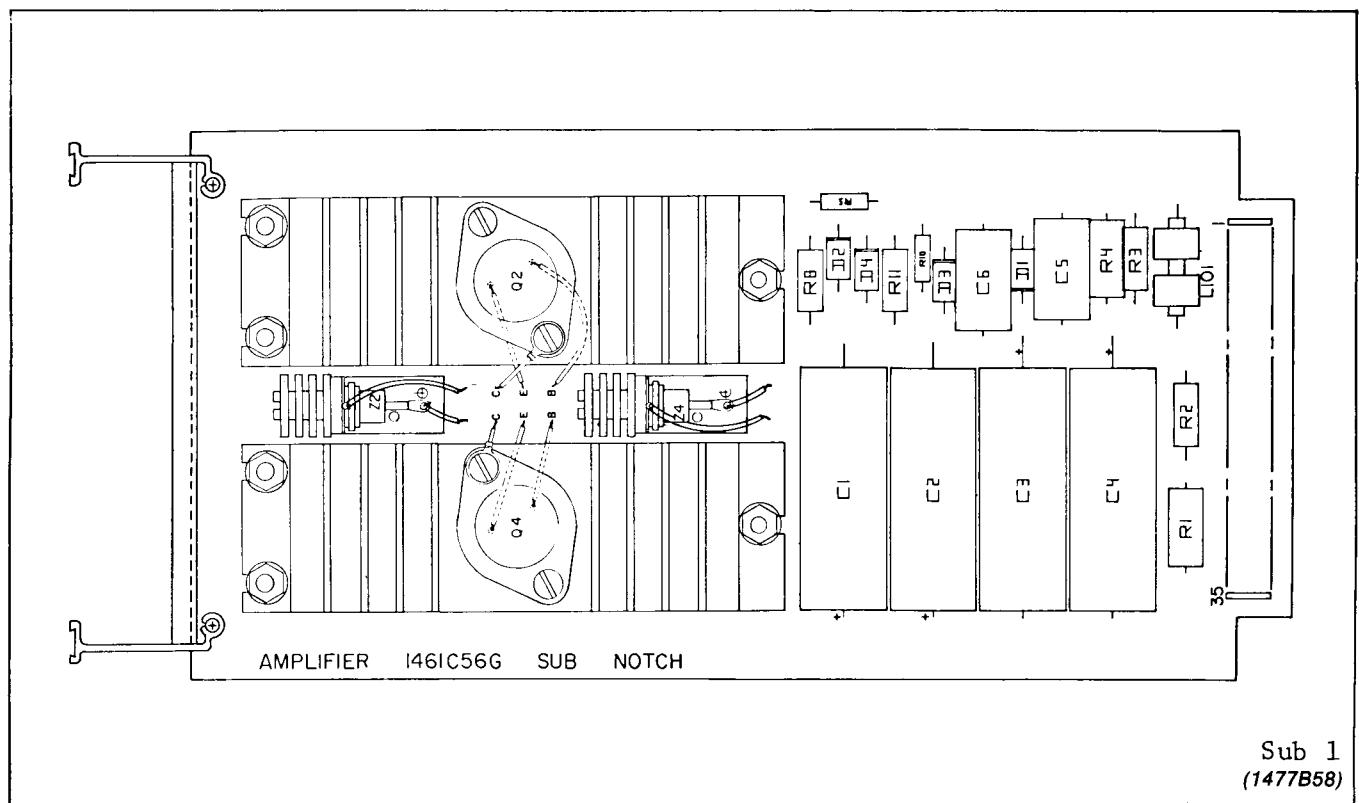


Fig. 11. Component Location Amplifier Board.

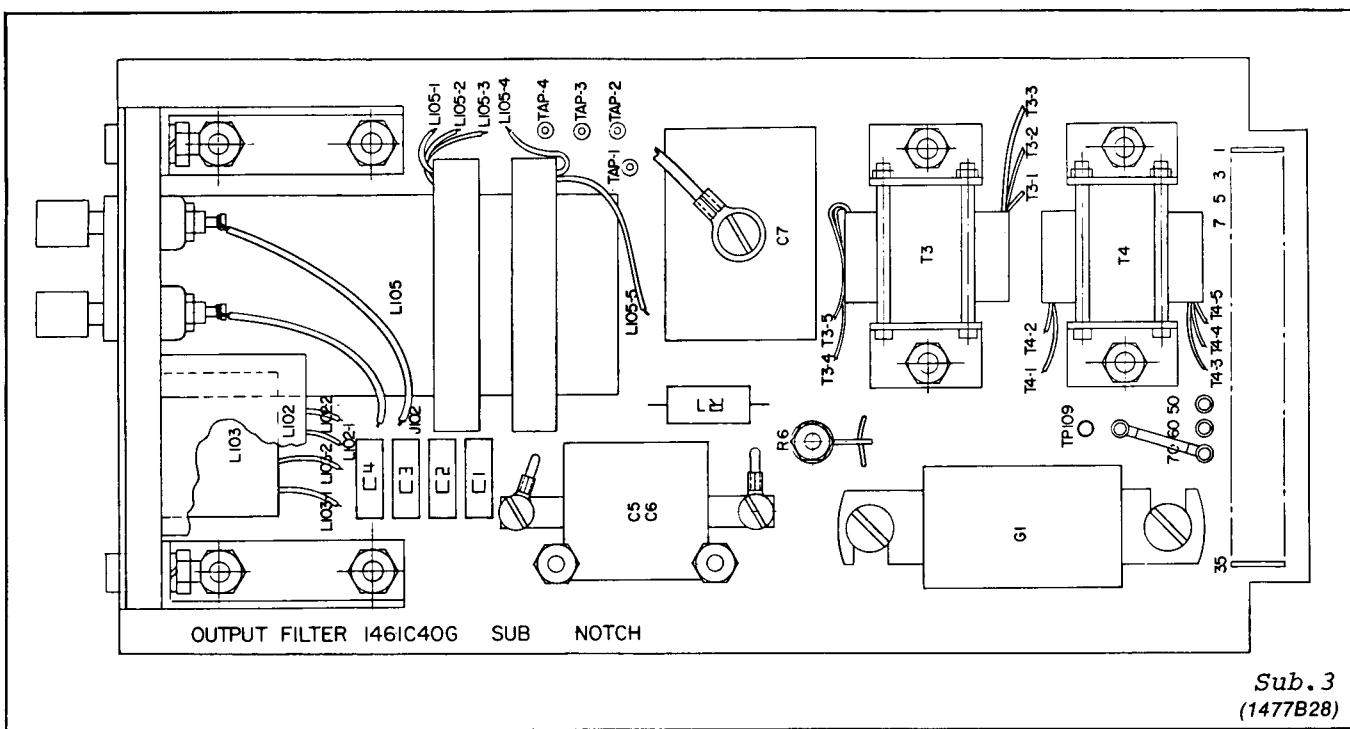


Fig. 12. Component Location Output Filter Board.

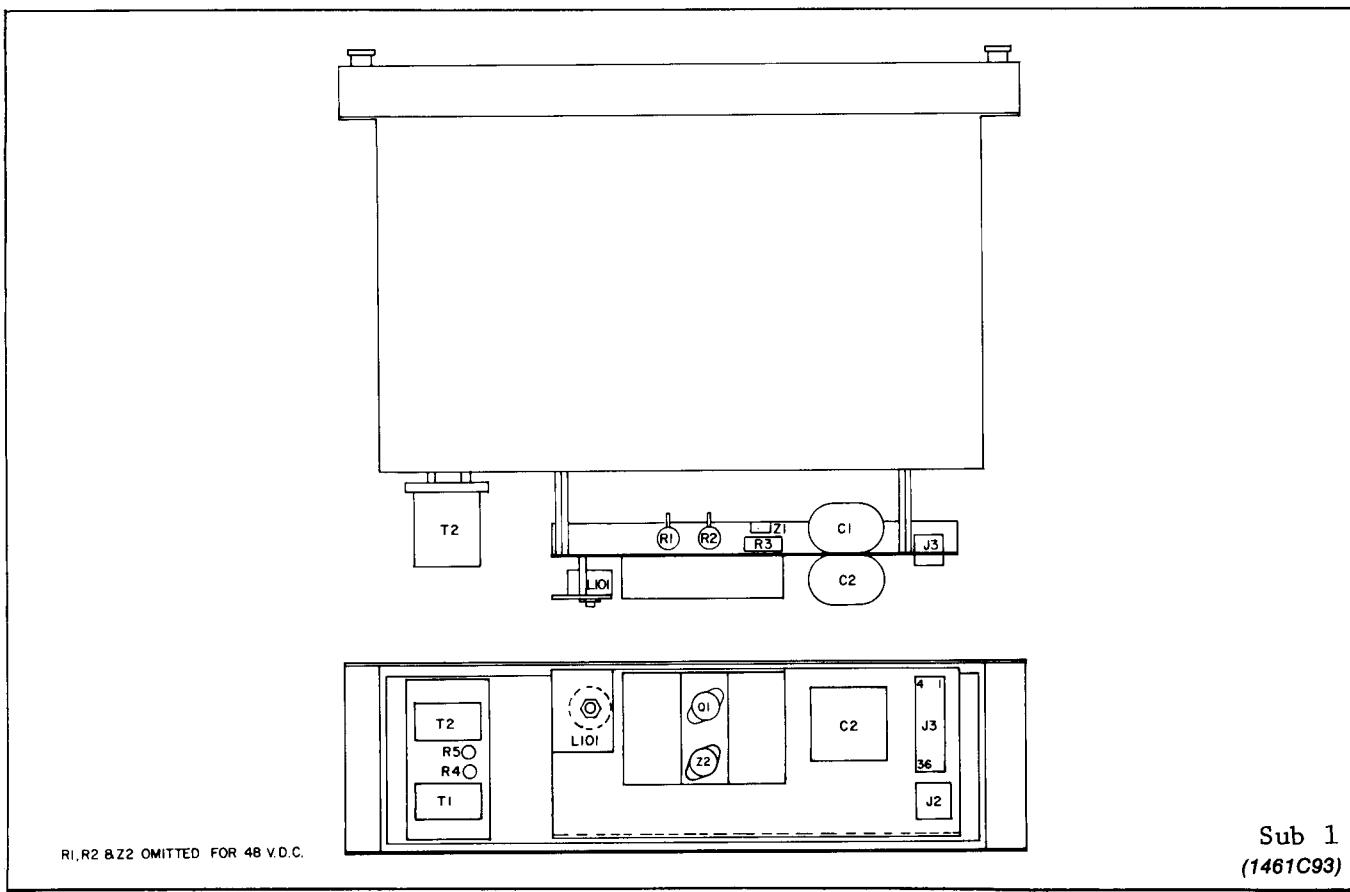


Fig. 13. Component Location Transmitter Assembly.

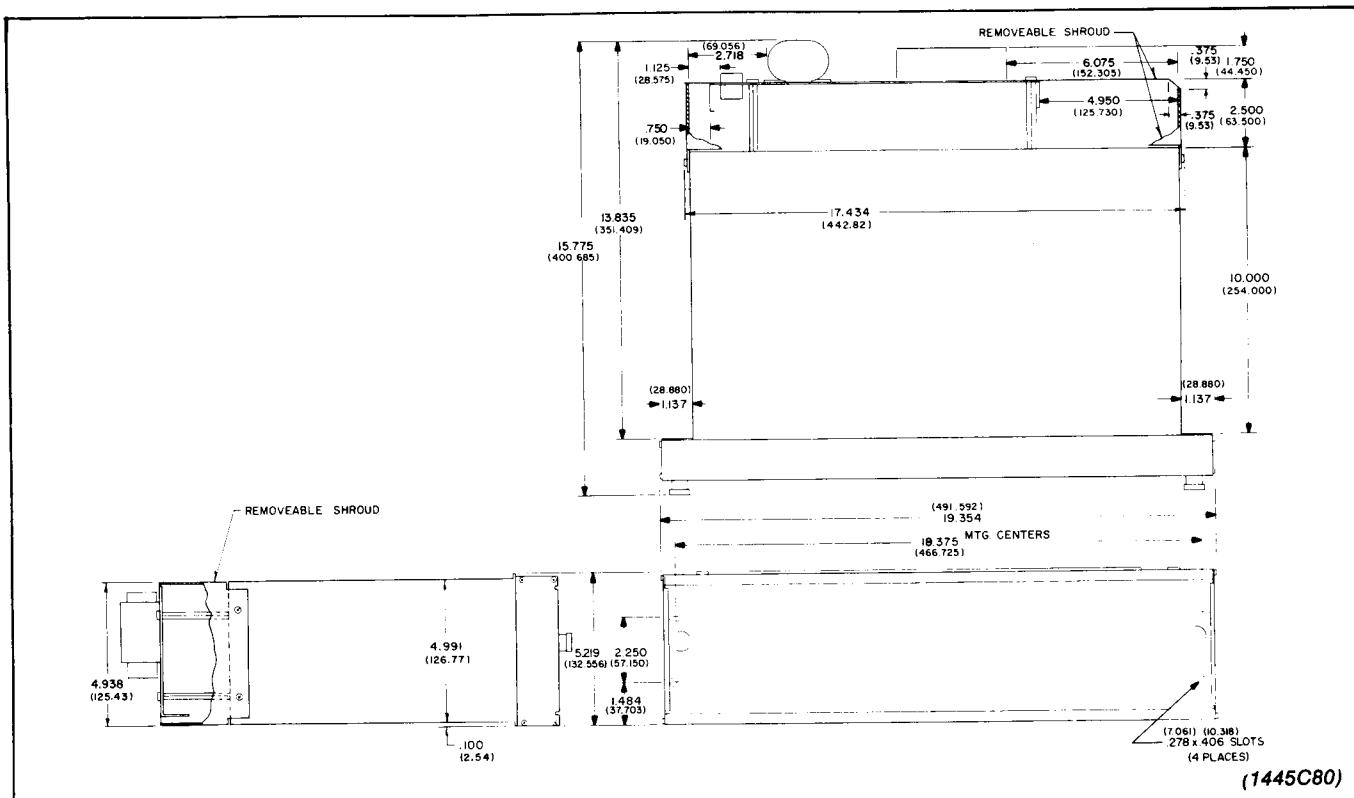


Fig. 14. Outline & Drilling for Transmitter Assembly.

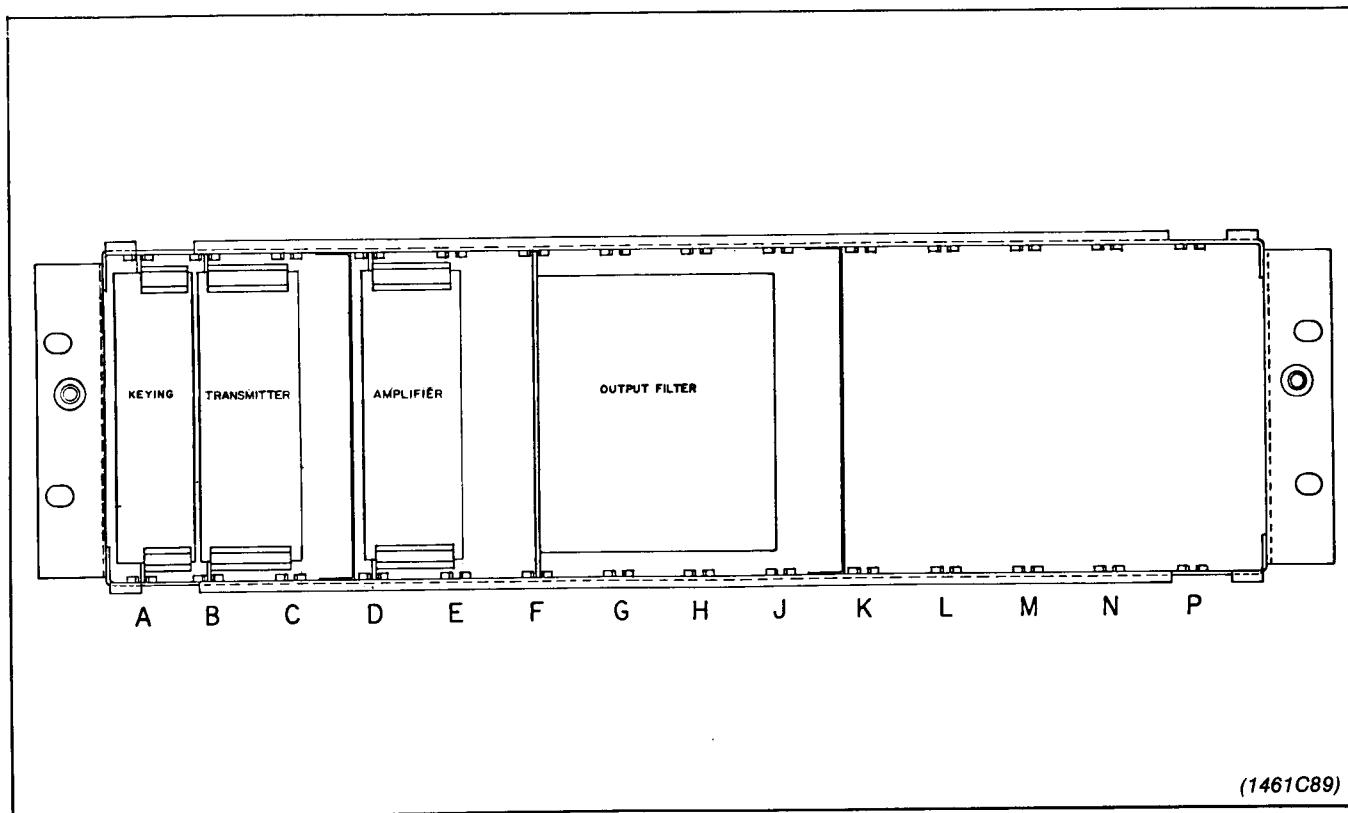
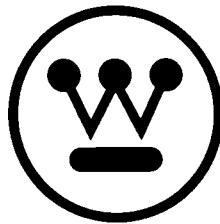


Fig. 15. Module Location.



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