

## Generator protection relay 7UM515

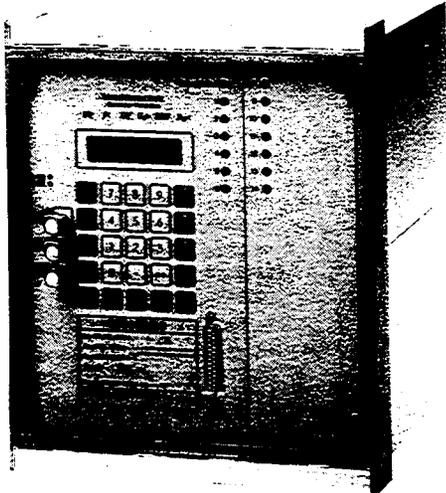


Fig. 1  
Generator protection relay 7UM515

### Application

The 7UM515 is a digital protection relay which is mainly used for larger generators in block connection. In the majority of cases it is used in combination with other units from the 7UM51 and 7UT51 series, whereby some functions can be used to provide redundant protection.

### Construction

The unit is of compact construction and comprises all components for:

- Measured value acquisition and evaluation
- Operator and display panel
- Alarm and command outputs
- Binary input options
- Serial interfaces
- Auxiliary voltage DC/DC converter.

Two casing models are available. The model for panel flush mounting or cubicle mounting has rear connection terminals. The model for panel surface mounting has 100 screw terminals accessible from the front.

### Protection functions

The unit contains the following integrated protection functions:

- 100 % stator earth-fault protection
- Rotor earth-fault protection (with 1 to 3 Hz bias)
- Earth-fault protection  $U_0 >$
- Interturn short-circuit protection  $U_w >$
- Overexcitation protection  $U/f$
- Overvoltage protection
- Undervoltage protection
- Overfrequency protection
- Underfrequency protection.

### Measurement method

The influence of superimposed harmonics and high-frequency transients is suppressed by the use of a powerful microprocessor and complete digital signal processing (measured value acquisition, measured value conditioning and measured value processing). High measurement accuracy is achieved by the use of process imaging based on physical models.

Operational readiness and correct measurement even with varying frequencies (during run-up and shut-down) are guaranteed by an automatic follow-up of the sampling frequency for the range of 10 to 70 Hz.

### Serial interfaces

The relay is equipped with two serial interfaces.

The operator interface at the front is suitable for connection of an AT-compatible personal computer. An operator program DIGSI is available for convenient and clear setting, evaluation of fault records and data, as well as for commissioning.

The system interface is either available as an isolated V. 24 interface or as a fibre optic interface for connection to the substation control system LSA 678 or to a central protection data unit (protocol according to DIN 19244).

### Settings

All setting parameters are input either via the integrated operator and display panel or a personal computer. The operator is guided through the setting process. The parameters are written into non-volatile memories so that the settings remain secure even when the supply voltage is disconnected.

### Self monitoring

All important hardware and software components are monitored continuously. Any irregularities in the hardware or in the program sequence are detected and alarmed. This significantly improves the security and the availability of the protection system.

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### 100 % stator earth-fault protection

In order to detect earth-faults in close proximity to the star point, a 20 Hz bias voltage is used as shown in Fig. 5. This voltage creates an earth current in the event of an earth fault.

The vector values ( $U_{20\text{Hz}}$ ;  $I_{20\text{Hz}}$ ) are determined from the input values  $U_{20\text{Hz}}$  and  $i_{20\text{Hz}}$  via a digital filter and used to calculate the fault resistance to earth. Frequencies deviating from 20 Hz are suppressed. If a correction angle is input, it is possible to compensate the phase-angle error of the current and voltage transformers as well as of the earthing or neutral earthing transformer.

The trip characteristic has two stages (alarm, trip).

A failure of the 20 Hz voltage is detected and the resistance measurement stopped. The earth-current supervision remains active and initiates an independent, time-delayed trip if the setting value is exceeded.

### Interturn short-circuit protection

The zero-sequence voltage is used to detect interturn short-circuits in generators. The fundamental wave is evaluated whereby harmonics are suppressed by filter algorithms. A matched input transmitter provides the high sensitivity.

Fig. 2 shows the basic connection for detecting interturn short-circuits. The star-point of the voltage transformer is connected via a high-voltage cable to the star-point of the generator. The voltage transformers must not be earthed on the primary side, since an "earth-fault" would lead to an earth short-circuit.

### Rotor earth-fault protection

This protection function detects earth-faults in the excitation circuit.

In order to eliminate the effect of earth capacitances in the excitation circuit, a DC voltage with constantly changing polarity (1 to 3 Hz) is connected via a series coupling unit to bias the excitation circuit. Thus, with each change in polarity, a charging current flows through the earth capacitances via the coupling unit and the measurement shunt. The voltage  $U_{\text{measured, REF}}$  measured at the measurement shunt, is filtered digitally in order to suppress interference values. The decayed measured voltage is used for resistance calculation.

Very large resistance values can thus be recognized independent of the location of the earth fault.

The trip characteristic is of two-stage design (alarm, short-time trip). Furthermore, the protection can be used to detect interruptions in the measurement circuit (e. g. transition between brushes and slip rings).

### Earth-fault protection

Earth-faults are detected by evaluating system-frequency neutral displacement voltages. In the example in Fig. 5, the protection detects earth-faults on the busbar section between the generator circuit-breaker and the auxiliary supply/block transformers when the generator circuit-breaker is open. If the generator circuit-breaker is closed, the earth-fault protection can also be used as a back-up protection for stator earth-faults. The voltage amplitude which can be evaluated provides protection of approximately 90 % of the stator winding.

By using a digital filter, the fundamental wave of the zero displacement voltage is evaluated and any harmonics are suppressed. Tripping can be time delayed.

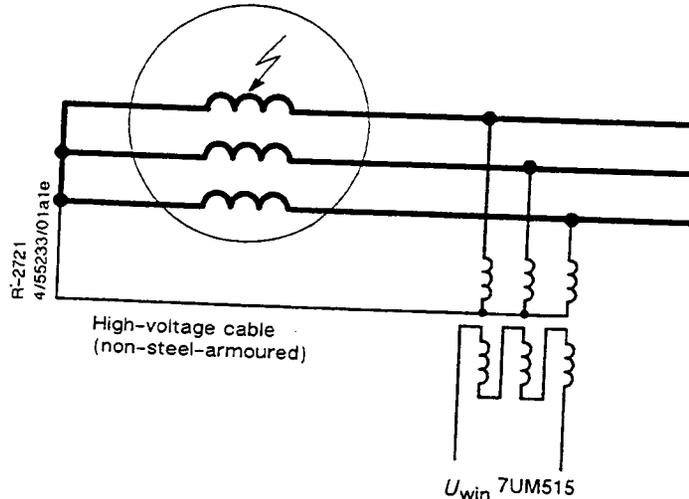


Fig. 2  
Block diagram of interturn short-circuit protection

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### Overexcitation protection

The overexcitation protection detects impermissibly high flux density in transformers, in particular in block transformers. This flux density is caused by a voltage increase and/or a frequency decrease, the consequence of which are saturation of the iron core and high eddy current losses.

Power station block transformers are particularly endangered when they are suddenly disconnected from the network at full load.

The overexcitation protection calculates the quotient of voltage and frequency which is proportional to the flux density. A thermal replica (1st order differential equation) is used to simulate the heating process. The permissible heating characteristic can be described by 6 sets of co-ordinates (intermediate values are interpolated). Thus, any  $U/f$  characteristic specified by the transformer manufacturer can be set. The alarm characteristic can be set as a percentage of the trip characteristic. In addition to the thermal characteristic, an adjustable, definite-time overexcitation stage (refer to Fig. 3) is also provided.

### Overvoltage protection, undervoltage protection

The three phase-to-phase voltages are measured and the fundamental wave is calculated by means of a digital filter.

The overvoltage protection evaluates the maximum phase-to-phase voltage in order to protect the generator and associated plant against impermissible voltage increases. The voltage increases can be caused by operator faults in case of manual voltage regulator operation or by faulty operation of the voltage regulator itself. The overvoltage protection has two stages.

Undervoltage protection is required in special cases (e. g. pumped storage stations) to ensure a timely disconnection of the generator from the network and to avoid voltage-induced network instability in the event of undervoltage.

The positive sequence system which is calculated from the filtered phase-to-phase voltages, is used for the evaluation. In order to facilitate matching to different applications, an inverse-time trip characteristic has been chosen (refer to Fig. 4). The characteristic can be described by 5 sets of co-ordinates.

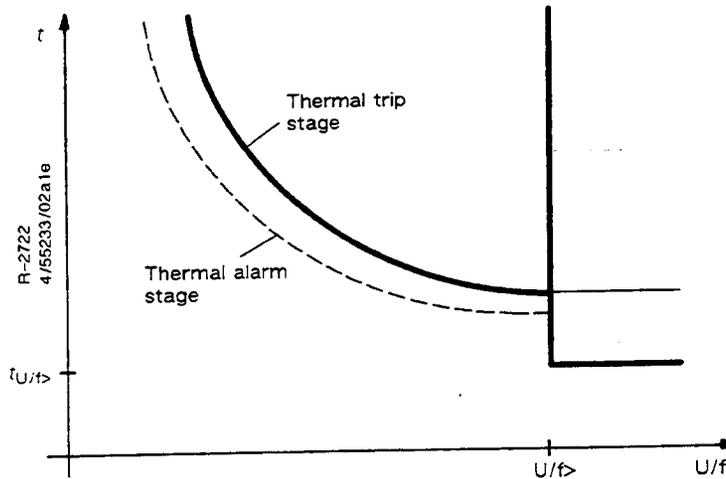


Fig. 3  
Trip characteristic of the overexcitation protection

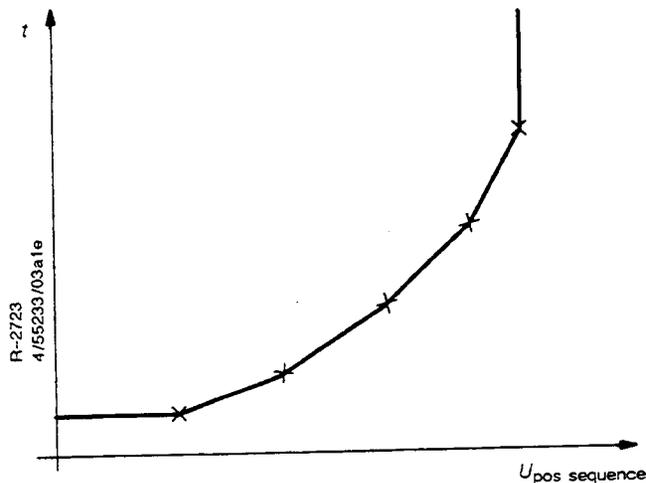


Fig. 4  
Trip characteristic of the undervoltage protection

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### Overfrequency protection, underfrequency protection

Generators, motors and consumers may only be operated within a limited frequency range. The frequency measurement uses the positive sequence voltage system and is based on zero crossing evaluation (fast underfrequency stage) and on evaluation of the angular speed of the positive sequence vector (extremely accurate frequency measurement).

Together with the fast underfrequency stage, an additional time stage can be activated. The extremely accurate frequency measurement is employed for two underfrequency stages and one overfrequency stage. The accuracy (operating range: 40 to 70 Hz) is further increased by an adjustable number of repeat measurements. Tripping is initiated when the counter status has been reached. A time delay can be realized at the same time.

### Assignable alarm relays/LED's

In order to provide a user-specific output and indication of alarms the assignment can be effected at liberty by the user.

### Trip matrix/trip circuits

The unit is equipped with five trip relays. These can be arbitrarily assigned to the above-mentioned protection functions by parameterization (software matrix).

Furthermore, each protection function can be switched "ON" or "OFF" via the operator panel. A third "Blocked" mode permits commissioning of the unit with the local annunciations and the alarm relay circuits operative, but without tripping of the circuit-breakers.

With the many parameterizing possibilities provided, testing of and alterations to the circuit-breaker operation can be performed during commissioning, as well as during normal operation without the need for rewiring.

### Fault event data

If a fault is detected in the protected object, the individual events and the train of measured data are stored in the unit. A choice can be made between recording either instantaneous or rms values.

These data can be read out via the serial interface. Evaluation of the data for fault analysis can then be performed by means of a PC program or a central data evaluation unit.

### On-load measurement

The on-load measured values generated in the relay such as voltages, frequency, stator earth current, earth resistances of stator and rotor can be displayed via the LCD display or a personal computer.

### Technical data

<b>Input circuits</b>	Rated voltage, can be parameterized Rated frequency, can be parameterized Burden in voltage path $U_N = 100\text{ V}$ Thermal overload capability in voltage paths in earth voltage path isolating amplifier Input resistance of isolating amplifier	90 to 125 V AC 50/60 Hz < 0.3 VA  140 V AC 140 V AC, 300 V AC for $\leq 30\text{ s}$ 60 V DC approx. 1 M $\Omega$
<b>Voltage supply</b> via integrated DC/DC converter	Rated auxiliary voltage $U_H$  Permissible tolerance Power consumption	24 V, 48 V DC or 60 V, 110 V, 125 V DC or 220 V, 250 V DC  -20 to +15 % max. 20 W
<b>Setting ranges</b> <b>100 % stator earth-fault protection</b>	Alarm stage $R <$ Trip stage $R \ll$ Earth current stage $I_{SEF} \gg$ Under-voltage blocking $U_{20} <$ Correction angle Delay times $t$ Reset delay $t_r$	20 to 500 $\Omega$ (secondary value) 10 to 300 $\Omega$ (secondary value) 0.02 to 0.8 A 0.5 to 15 V -15 to +15° 0 to 60 s 0 to 60 s
<b>Rotor earth-fault protection</b>	Alarm stage $R_E <$ Trip stage $R_E \ll$ Delay times $t$ Reset delay $t_r$	5 to 80 k $\Omega$ 0.5 to 10 k $\Omega$ 0 to 60 s 0 to 60 s
<b>Earth-fault protection</b>	Displacement voltage $U_0 >$ Delay time $t$ Reset delay $t_r$	5 to 120 V AC 0 to 60 s 0 to 60 s

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### Technical data (contin.)

<b>Setting ranges</b> <b>Interturn short-circuit protection</b>	Displacement voltage $U_W >$ Delay time $t$ Reset delay $t_r$	0.3 to 16 V AC 0 to 60 s 0 to 60 s
<b>Overexcitation protection</b>	Overexcitation $\frac{U/U_N}{t/t_N} >$ Delay time $t$ Reset delay $t_r$ U/f characteristic Co-ordinates U/f Associated times Time factor U/f basis Alarm stage	1 to 1.5 0 to 60 s 0 to 60 s 1.02 to 1.6 1 to 98 s 1 to 8 0 to 1 70 % to 100 % of U/f characteristic
<b>Overvoltage protection, undervoltage protection</b>	Overvoltage $U >, U \gg$ Delay time $t$ Undervoltage characteristic Co-ordinates $U <$ Associated times Reset delay $t_r$	50 to 140 V 0 to 60 s 5 to 95 V 0.1 to 30 s 0 to 60 s
<b>Overfrequency protection, underfrequency protection</b>	Overfrequency $f >$ Underfrequency $f_1, f_2 <$ Number of repeat measurements $f <, f >$ Time delay Undervoltage blocking for $f <, f >$ Underfrequency $f \ll$ Delay time $t (f \ll)$ Reset delay $t_r (f \ll)$	40 to 65 Hz 40 to 65 Hz 5 to 100 1 repeat measurement $\Delta$ 60 ms at 50 Hz 40 to 100 V 35 to 65 Hz 0 to 60 s 0 to 60 s
<b>Pick-up tolerances</b>	100 % stator earth-fault protection $R <, R \ll$ $I_{SEF} \gg$ Rotor earth-fault protection $R_E <, R_E \ll$ Earth-fault protection $U_0 >$ Interturn short-circuit protection $U_W >$ Overexcitation protection U/f starting U/f characteristic Overvoltage and undervoltage protection Frequency protection $f >, f <$ $f \ll$ Delay times	5 % of set value or 2 $\Omega$ 3 % of set value or 3 mA 5 % of set value or 500 $\Omega$ 3 % of set value 3 % of set value or 0.1 V 5 % of set value 5 % referred to U/f set value 3 % of set value or 1 V 10 mHz at $f > f_N$ 100 mHz 1 % or 10 ms
<b>On-load measurement</b>	Indication of values for voltages for current for resistance for frequency for overexcitation for calculated temperature during overexcitation	$U_{L1}, U_{L2}, U_{L3}, U_{max LL},$ $U_{pos sequence}, U_0, U_W, U_{SEF}$ $I_{SEF}$ $R_{SEF}, R_{REF}$ $f$ $\frac{U/U_N}{t/t_N}$ thermal replica
<b>Fault recording</b>	Instantaneous values rms values	approx. every 1.67 ms at 50 Hz $U_{L1}, U_{L2}, U_{L3}, U_0, U_{REF}, U_W, U_{SEF}, I_{SEF}$ approx. every 10 ms $f, U_{LL}, U_0, U_{pos sequence}, U_W, U_{SEF}, I_{SEF}, R_{SEF}$





Dimension drawings in mm

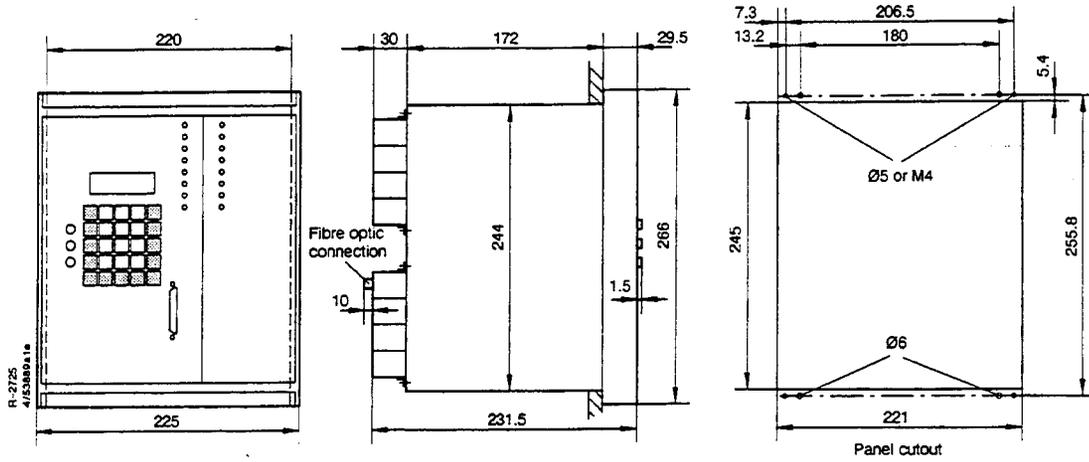


Fig. 6  
Panel flush mounting, cubicle mounting

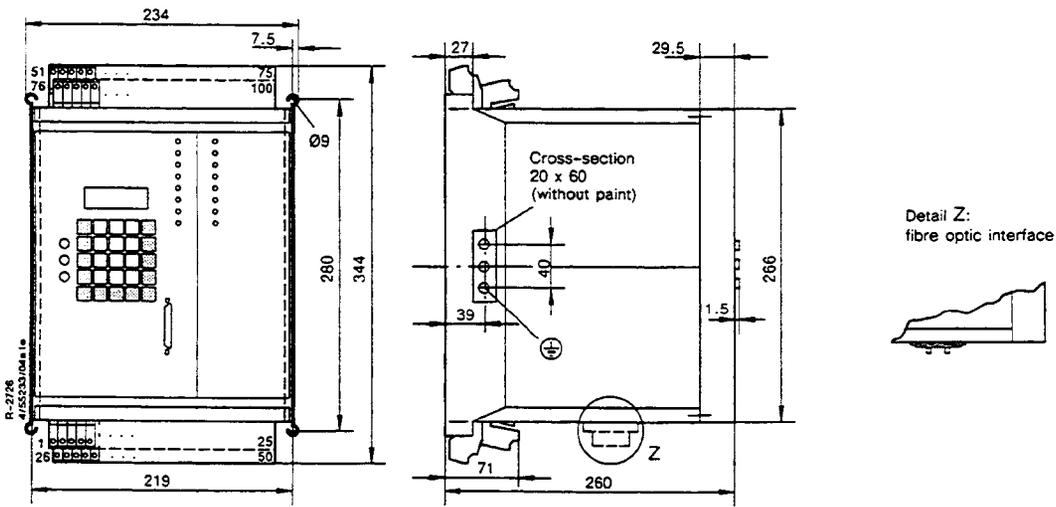


Fig. 7  
Panel surface mounting





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